



A Solution of the Alekseevski-Tate Penetration Equations

by William Walters and Cyril Williams

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14. ABSTRACT <p>The Alekseevski-Tate equations have been used for five decades to predict the penetration, penetration velocity, rod velocity, and rod length of long-rod penetrators and similar projectiles. These nonlinear equations were originally solved numerically and more recently by the exact analytical solution of Walters and Segletes. However, due to the nonlinear nature of the equations, penetration was obtained implicitly as a function of time. The current report obtains the velocities, length, and penetration as an explicit function of time by employing a perturbation solution of the nondimensional Alekseevski-Tate equations. Explicit analytical solutions are advantageous in that they clearly reveal the interplay of the various parameters on the solution of the equations. Perturbation solutions of these equations were first undertaken by Forrestal et al., up to the first order, and good agreement with the exact solutions was shown for relatively short times. The current study obtains a third-order perturbation solution and includes both penetrator and target strength terms. This report compares the exact solution to the perturbation solution, and a typical comparison between the exact and approximate solution for a tungsten rod impacting a steel armor target is shown. Also, alternate ways are investigated to normalize the governing equations in order to obtain an optimum perturbation parameter. In most cases, the third-order perturbation solution shows near perfect agreement with the exact solutions of the Alekseevski-Tate equations. This report compares the exact solution to the perturbation solution, and comments are made regarding the range of validity of the explicit solution.</p>					
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1. Introduction

The Alekseevski-Tate equations (1) have long been employed to predict the penetration of kinetic energy penetrators or rod-like projectiles. Typically, these equations are solved by straight-forward numerical integration techniques or by using the exact solution developed by Walters and Segletes (2) and refined by Segletes and Walters (3). However, due to the nonlinear nature of these equations, the exact solution yields penetration only as an implicit function of time. It is desirable to obtain an exact, albeit approximate, solution to these equations which would yield the pertinent variables, penetration velocity, penetrator length, penetrator velocity, and penetration as an explicit function of time. The analytical nature of the solutions would clearly reveal the interplay of the various terms in the governing equations on the solutions. Toward this end, as per references (1–2), a perturbation solution was obtained for the following equation set:

$$(\rho_P/2)(v-u)^2 + Y_P = (\rho_T/2)u^2 + R_T \quad (1)$$

$$\frac{dv}{dt} = \frac{-Y_P}{l\rho_P} \quad (2)$$

$$\frac{dl}{dt} = u - v \quad (3)$$

$$u = \frac{dp}{dt} \text{ or } p = \int u dt . \quad (4)$$

In these equations, v is the penetrator velocity, u is the penetration velocity, p is the penetration, l is the penetrator length, t is the time after impact, R_T is the target strength term, Y_P is the penetrator strength term, ρ represents the density, where the subscript P stands for penetrator and subscript T represents the target. First, the equations are normalized and the method of normalization will depend on the input conditions; namely, the ρ values, the initial velocity, and the strength terms. For the usual case of interest to ballisticians studying kinetic energy penetrators impacting armor targets, the following normalization parameters are introduced:

$$V = v/V_i, \quad U = u/V_i, \quad \lambda = l/L, \quad \tau = \beta t, \text{ and} \quad (5)$$

$$\mu^2 = \rho_T/\rho_P, \quad \beta = \left(\frac{\mu}{1+\mu} \right) \frac{V_i}{L}, \quad \alpha = \frac{R_T - Y_P}{Y_P}, \quad \varepsilon = \frac{Y_P}{\rho_P V_i^2}, \quad P = \frac{p}{L}, \quad (6)$$

where V_i is the impact velocity, L is the initial penetrator length, and V , U , P , λ , and τ are the dimensionless variables, while μ , α , β , and ε are the dimensionless constants. The parameter β is used to normalize the time. The constant ε is the perturbation parameter. This is the same

normalization scheme used by Forrestal et al. (4). Forrestal et al. assumed $R_T = 0$ (i.e., $\alpha = -1$) for a steel projectile impacting a foundry core target (silica sand) at 3.0 km/s.

Thus, the normalized equations become

$$(V - U)^2 - 2\alpha\varepsilon = \mu^2 U^2, \quad (7)$$

$$\frac{dV}{d\tau} = -\frac{\varepsilon}{\lambda} \left(\frac{1+\mu}{\mu} \right), \quad (8)$$

$$\frac{d\lambda}{d\tau} = \left(\frac{1+\mu}{\mu} \right) (U - V), \quad (9)$$

and

$$P = \left(\frac{1+\mu}{\mu} \right) \int_0^\tau U d\tau. \quad (10)$$

The perturbation method, as shown by Cole (5), involves letting

$$V = V_0 + \varepsilon V_1 + \varepsilon^2 V_2 + \varepsilon^3 V_3 + \dots \quad (11)$$

$$U = U_0 + \varepsilon U_1 + \varepsilon^2 U_2 + \varepsilon^3 U_3 + \dots \quad (12)$$

$$\lambda = \lambda_0 + \varepsilon \lambda_1 + \varepsilon^2 \lambda_2 + \varepsilon^3 \lambda_3 + \dots \quad (13)$$

$$P = P_0 + \varepsilon P_1 + \varepsilon^2 P_2 + \varepsilon^3 P_3 + \dots \quad (14)$$

and the perturbation parameter $\varepsilon = \frac{Y_P}{\rho_P V_i^2} \ll 1$ is chosen.

For example, if a third-order perturbation solution is obtained, terms of the order of ε to the fourth power are neglected. Hence, the accuracy of the solution depends on the magnitude of ε and the number of terms in the above equation set.

One can substitute the expressions for V , U , λ , and P (equations 11–14) into the nondimensional equation set (equations 7–10) and obtain, to order zero (considering only terms involving ε^0), the following set:

$$(V_0 - U_0)^2 = \mu^2 U_0^2, \quad (15)$$

$$\frac{dV_0}{d\tau} = 0, \quad (16)$$

and

$$\frac{d\lambda_0}{d\tau} = -\left(\frac{1+\mu}{\mu} \right) (V_0 - U_0), \quad (17)$$

where the initial conditions at $\tau = 0$ are $V_0(0) = 1$, $\lambda_0(0) = 1$.

The solution is

$$V_0 = 1 , \quad (18)$$

$$U_0 = \frac{1}{1+\mu} , \quad (19)$$

$$\lambda_0 = 1 - \tau , \quad (20)$$

and

$$P_0 = \frac{\tau}{\mu} , \quad (21)$$

in agreement with Forrestal et al. (4).

Proceeding along these same lines (next consider terms of order ε , etc.), one can calculate V_0 , V_1 , V_2 , V_3 , and the corresponding U , P , and λ values. The method is straight forward but tedious. The final equations, to the third order, are

$$V = V_0 + \varepsilon V_1 + \varepsilon^2 V_2 + \varepsilon^3 V_3 , \quad (22)$$

$$U = U_0 + \varepsilon U_1 + \varepsilon^2 U_2 + \varepsilon^3 U_3 , \quad (23)$$

$$\lambda = \lambda_0 + \varepsilon \lambda_1 + \varepsilon^2 \lambda_2 + \varepsilon^3 \lambda_3 , \quad (24)$$

and

$$P = P_0 + \varepsilon P_1 + \varepsilon^2 P_2 + \varepsilon^3 P_3 , \quad (25)$$

where

$$V_1 = \Theta \ln \Pi ,$$

$$V_2 = \Theta^2 \Omega \left[\ln \Pi + \frac{1}{\Pi} - 1 \right] - \frac{1}{2} \Theta^2 [\ln \Pi]^2 ,$$

$$V_3 = \Theta^3 \left[\Psi \ln \Pi - \frac{\Omega^2}{2\Pi^2} + \left(2\Omega + 2\Omega^2 - \frac{\alpha^2}{2\mu} + \frac{\alpha^2}{2\mu^2} \right) \frac{1}{\Pi} - 2\Omega (\ln \Pi)^2 + \frac{1}{2} (\ln \Pi)^3 - \Omega \frac{\ln \Pi}{\Pi} + C_3 \right] ,$$

$$U_1 = \left(\frac{1}{\mu} \right) [\ln \Pi - \alpha] ,$$

$$U_2 = \frac{V_2}{1+\mu} + \frac{\alpha}{\mu^2} (1+\mu) \ln \Pi + \frac{\alpha^2}{2\mu^3} (1-\mu^2) ,$$

$$U_3 = \frac{V_3}{1+\mu} - \frac{\alpha \Theta^2}{\mu} \left[\frac{3(\ln \Pi)^2}{2} + \left(\frac{3}{2} - \frac{5\Omega}{2} - \frac{3\alpha}{2} \right) \ln \Pi - \frac{\Omega}{\Pi} + \left(\frac{1}{2} \left(\frac{\alpha}{\mu} (1-\mu) \right)^2 + \Omega \right) \right] ,$$

$$\lambda_1 = \Theta [\tau \Omega + \Pi \ln \Pi] ,$$

$$\lambda_2 = \Theta^2 \left[- \left(3 - \frac{3\alpha}{\mu} - \frac{\alpha^2}{2\mu} + \frac{\alpha^2}{2\mu^2} \right) \Pi + \Omega \ln \Pi + 2\Omega \Pi \ln \Pi - \frac{1}{2} \Pi (\ln \Pi)^2 + C_{\lambda_2} \right] ,$$

$$\lambda_3 = \Theta^3 \left[- \frac{7\Omega}{2} \Pi (\ln \Pi)^2 + \Sigma \ln \Pi + \Phi \Pi \ln \Pi + \Gamma \Pi - \frac{\Omega}{2} (\ln \Pi)^2 + \frac{\Omega^2}{2\Pi} + \frac{\Pi (\ln \Pi)^3}{2} \right] + C_{\lambda_3} ,$$

$$P_1 = - \frac{\Theta}{\mu} \left[\tau(1+\alpha) + \Pi \ln \Pi \right] ,$$

$$P_2 = \frac{\Theta^2}{\mu} \left[\left(3 + \alpha + \frac{\alpha^2}{2} - \frac{2\alpha}{\mu} - \frac{\alpha^2}{2\mu} \right) \Pi - \Omega \ln \Pi - \left(2 + \alpha - \frac{\alpha}{\mu} \right) \Pi \ln \Pi + \frac{1}{2} \Pi (\ln \Pi)^2 \right] + C_{P_2} ,$$

$$P_3 = - \frac{\Theta^3}{\mu} \left[\left(\xi - \frac{\Omega^2}{2} \right) \Pi + \omega \Pi \ln \Pi + \frac{\Omega^2}{2\Pi} + \vartheta \ln \Pi + \delta \Pi (\ln \Pi)^2 - \frac{\Omega}{2} (\ln \Pi)^2 + \frac{1}{2} \Pi (\ln \Pi)^3 \right] + C_{P_3} ,$$

and

$$\Psi = \left(4 - \frac{5\alpha}{\mu} - \frac{\alpha^2}{2\mu} + \frac{3\alpha^2}{2\mu^2} \right) ,$$

$$\Pi = 1 - \tau ,$$

$$\Theta = \frac{(1+\mu)}{\mu} ,$$

$$\Omega = 1 - \frac{\alpha}{\mu} ,$$

$$C_3 = - \frac{3\Omega^2}{2} - 2\Omega - \frac{1}{2} \left(\frac{\alpha}{\mu} \right)^2 (1-\mu) ,$$

$$\Sigma = \frac{7\Omega^2}{2} - \frac{\alpha^2}{2\mu} + \frac{1}{2} ,$$

$$\Phi = 2 + 5\Omega + 4\Omega^2 - \frac{2\alpha^2}{\mu} ,$$

$$\Gamma = - \frac{5}{2} - 7\Omega^2 - 5\Omega + \frac{5\alpha^2}{2\mu} + \frac{\alpha^3}{2\mu^3} (\mu-1)^2 ,$$

$$\xi = -4 - 3\Omega^2 - 7\Omega + \frac{9\alpha^2}{2\mu} - 5\alpha - \frac{3\alpha^2}{2} - \frac{\alpha^3}{2\mu^2} (1-\mu)^2 ,$$

$$\omega = \frac{7}{2} + 6\Omega + 3\alpha\Omega + \frac{3\Omega^2}{2} + \alpha + \frac{3\alpha^2}{2} ,$$

$$\mathcal{G} = \Omega + \frac{5\Omega^2}{2} + \alpha - \frac{3\alpha^2}{2\mu} + \frac{1}{2} ,$$

$$\delta = -2\Omega - \frac{3}{2}(1 + \alpha) ,$$

$$C_{\lambda_2} = 3 - \frac{3\alpha}{\mu} - \frac{\alpha^2}{2\mu} + \frac{\alpha^2}{2\mu^2} ,$$

$$C_{\lambda_3} = \Theta^3 \left(\frac{5}{2} + \frac{13\Omega^2}{2} + 5\Omega - \frac{5\alpha^2}{2\mu} - \frac{\alpha^3}{2\mu^3} (\mu - 1)^2 \right) ,$$

$$C_{P2} = -\frac{\Theta^2}{\mu} \left(3 + \alpha + \frac{\alpha^2}{2} - \frac{2\alpha}{\mu} - \frac{\alpha^2}{2\mu} \right) ,$$

and

$$C_{P3} = \frac{\Theta^3 \xi}{\mu} .$$

The normalization scheme used is deemed appropriate for ballistic applications, namely tungsten rods penetrating steel. The third-order solution for U , V , P , and λ , with comparison to the exact Alekseevski-Tate equation solution, is shown in figures 1–3. In this case, $V_i = 2$ km/s, $L = 0.5$ m, $\rho_p = 17,600$ kg/m³, $Y_p = 1.0$ GPa, $\rho_t = 7,800$ kg/m³, and $R_t = 5.5$ GPa. The perturbation parameter computes as $\varepsilon = 0.0142$, which is much less than one and terms with a coefficient of ε^4 were neglected. The agreement is excellent up to about 495 μ s for the velocities and nearly identical for the rod length and penetration. The exact (Tate) solution terminates at about 518 μ s. The appendix lists the FORTRAN program used to calculate the rod velocity, penetration velocity, rod length, and penetration all as a function of time.

A few comments are in order. All equations contain a term like $\ln(1-\tau)$. Thus, a singularity occurs at $\tau = 1$ or $t = \frac{L(1+\mu)}{\mu V_i} = 625.5$ μ s for the case described. Thus, t must be less than this

value for the perturbation solution to be evaluated. As this singularity is approached, deviation from the exact solution occurs. Hence, one can accurately calculate the perforation of finite thickness targets if the penetration time is less than this value. As an example, figures 4–6 plot the rod velocity, penetration velocity, penetration, and rod length for a tungsten rod impacting a finite-thickness (25 mm) steel plate as described, except the initial rod length was 39.12 mm. The first-order and third-order perturbation theories are compared with the Tate solution. Again, the agreement is excellent. Note that the first-order perturbation theory also agrees very well with the exact solution for this case. Thus, approximate formulae may be derived for the perforation of thin plates. The first order equations are

$$V = 1 + \varepsilon \Theta \ln \Pi , \tag{26}$$

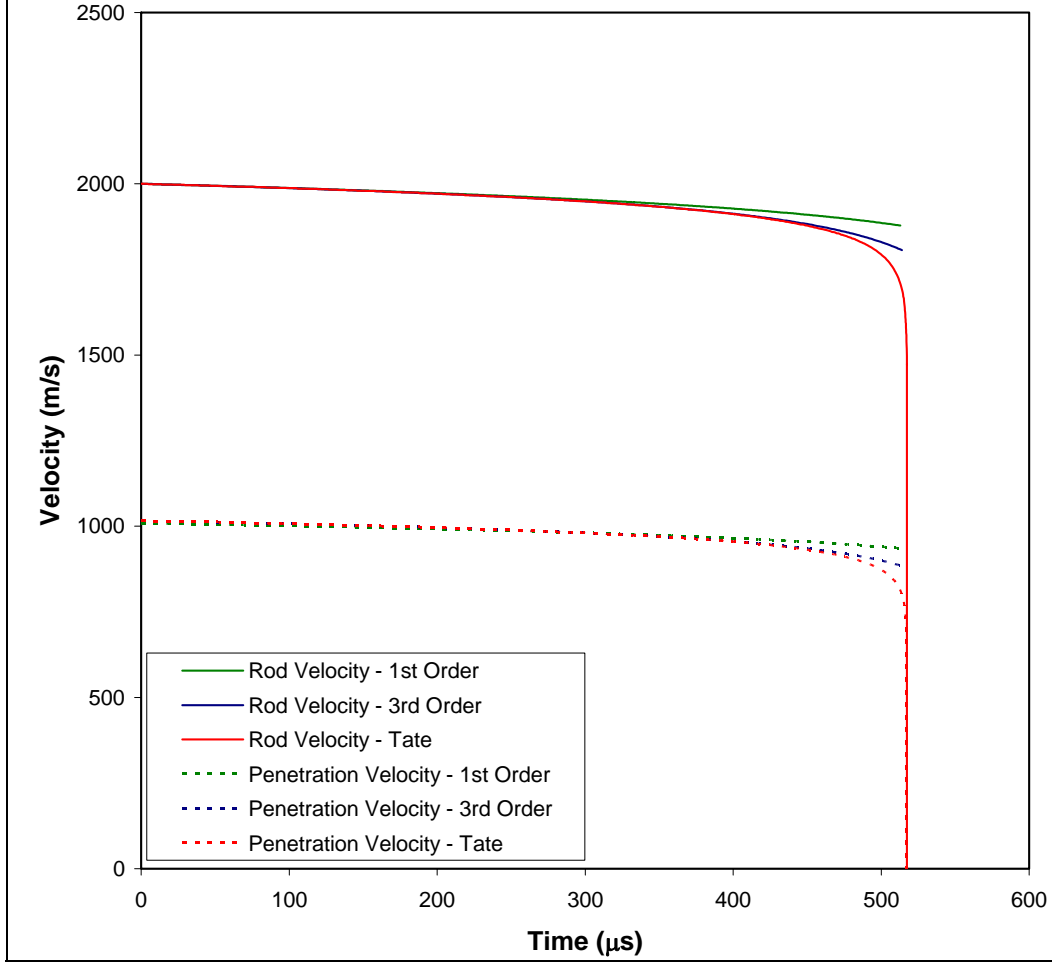


Figure 1. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

$$U = \frac{1}{1+\mu} + \frac{\varepsilon}{\mu} [\ln \Pi - \alpha] , \quad (27)$$

$$\lambda = \Pi + \varepsilon \Theta [\Omega(1-\Pi) + \Pi \ln \Pi] , \quad (28)$$

and

$$P = \frac{1-\Pi}{\mu} - \frac{\varepsilon \Theta}{\mu} [(1-\Pi)(\alpha+1) + \Pi \ln \Pi] . \quad (29)$$

When $P=H$, the finite target plate thickness, equation 29 can be solved for the event duration in terms of Π as

$$\Pi = \exp \left[\frac{-1}{A\Pi} \left(\frac{H}{L} + \frac{\Pi-1}{\mu} \right) - \frac{(1-\Pi)}{\Pi} (\alpha+1) \right] \text{ and } A = \frac{\varepsilon \Theta}{\mu} . \quad (30)$$

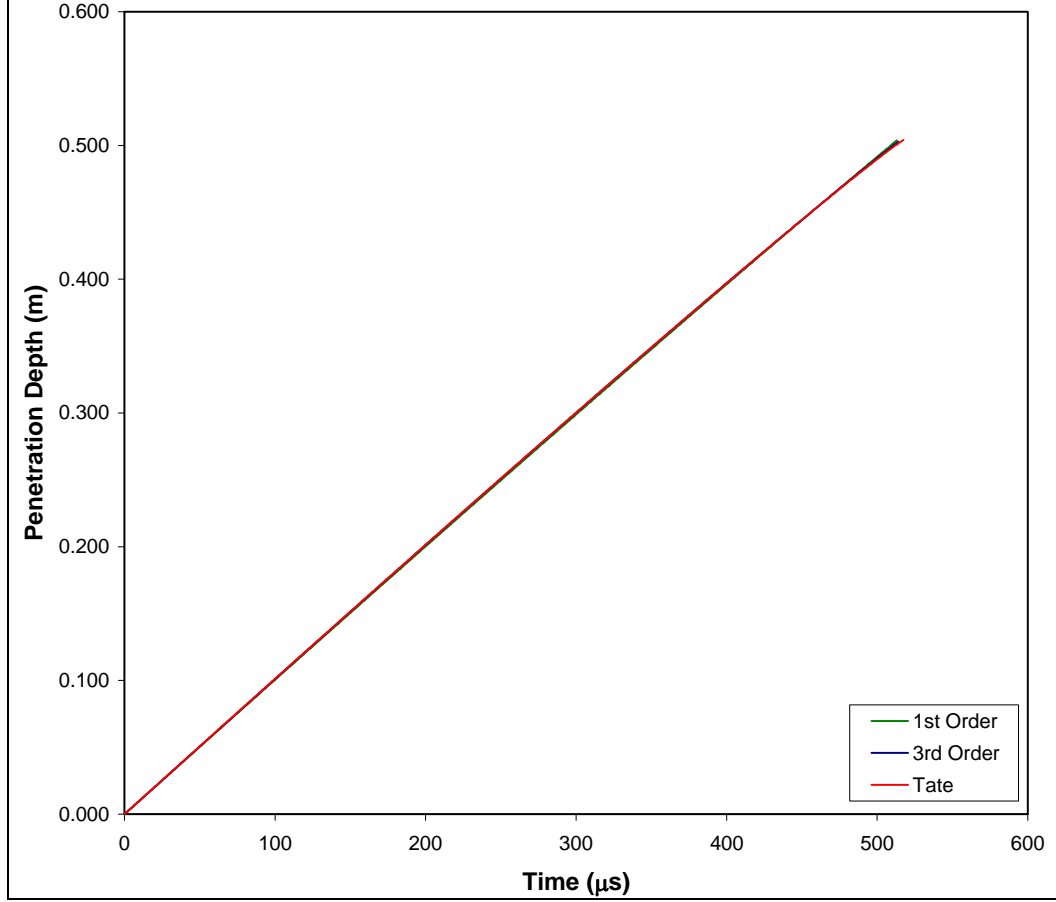


Figure 2. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

Further, the exponential term in equation 30 may be approximated by the first two terms of its series expansion or $\exp[x] = 1 + x$. In this case,

$$\Pi = \frac{B + \sqrt{B^2 + 4C}}{2} \text{ where } B = 2 + \alpha - \frac{1}{A\mu} \text{ and } C = -\frac{H}{AL} + \frac{1}{A\mu} - (\alpha + 1). \quad (31)$$

From equation 31, the time, t , was 25.34 μs and the time calculated from the more exact equation 30 via standard iteration techniques was 25.12 μs . The rod velocity was 1948.156 m/s according to the approximate theory and 1943.000 m/s from the Tate solution. The penetration velocity was 977.524 m/s vs. 976.500 m/s from the Tate solution. The final rod length was 14.20 mm vs. 14.70 mm from the Tate solution. This close agreement means that the perturbation solution is in excellent agreement with the Tate solution for small times, even for a first-order perturbation solution. Forrestal et al. (4) also showed good agreement with Tate for short times.

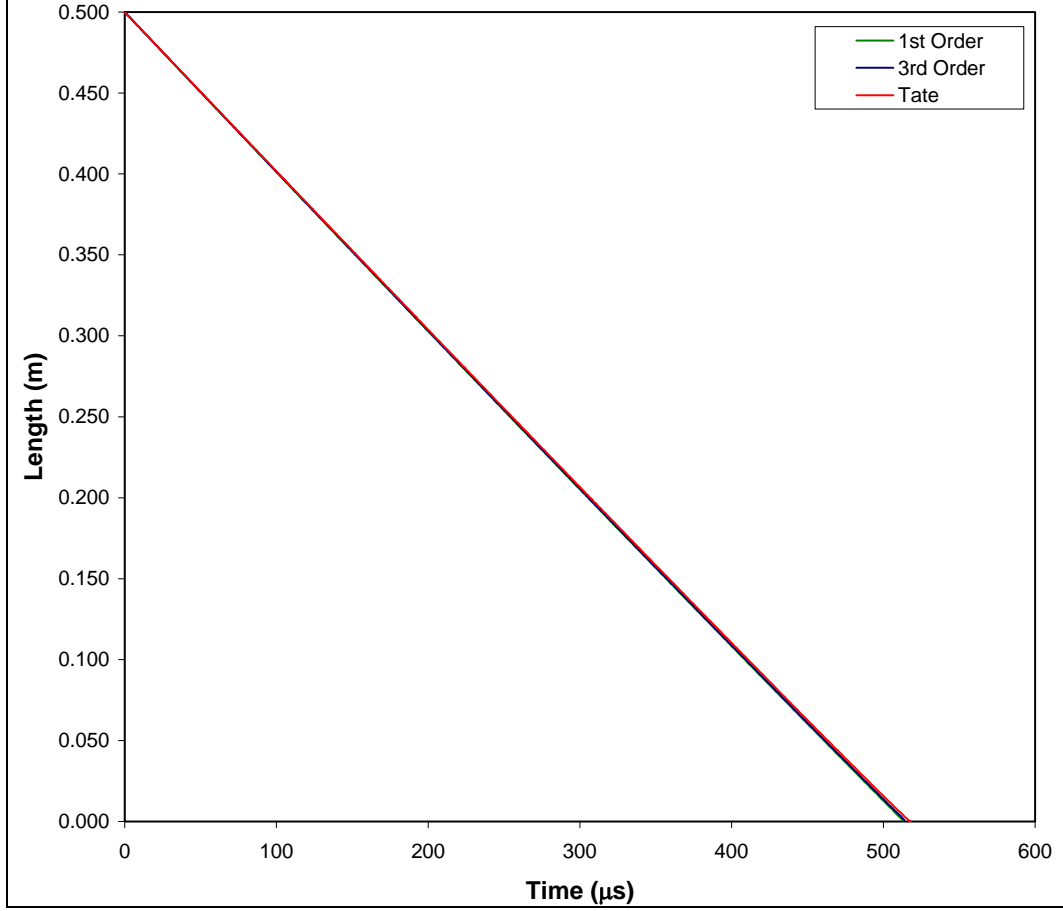


Figure 3. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

As previously mentioned, the perturbation parameter must be much less than one. The value of ε used in the above equations implies a small penetrator strength or $Y_p \ll \rho_p V_i^2$. If this is not the case, for example, for a soft target, i.e., small R_T , the equations can be normalized with

$$V = v/V_i, \quad U = u/V_i, \quad \lambda = l/L, \quad P = \frac{p}{L}, \quad (32)$$

$$\mu^2 = \rho_T / \rho_P, \quad \beta = \left(\frac{\mu}{1 + \mu} \right) \frac{V_i}{L}, \quad \alpha = \frac{Y_p - R_T}{R_T}, \quad \varepsilon = \frac{R_T}{\rho_P V_i^2}, \quad \tau = \beta t, \quad (33)$$

and the equation set becomes

$$(V - U)^2 + 2\alpha\varepsilon = \mu^2 U^2, \quad (34)$$

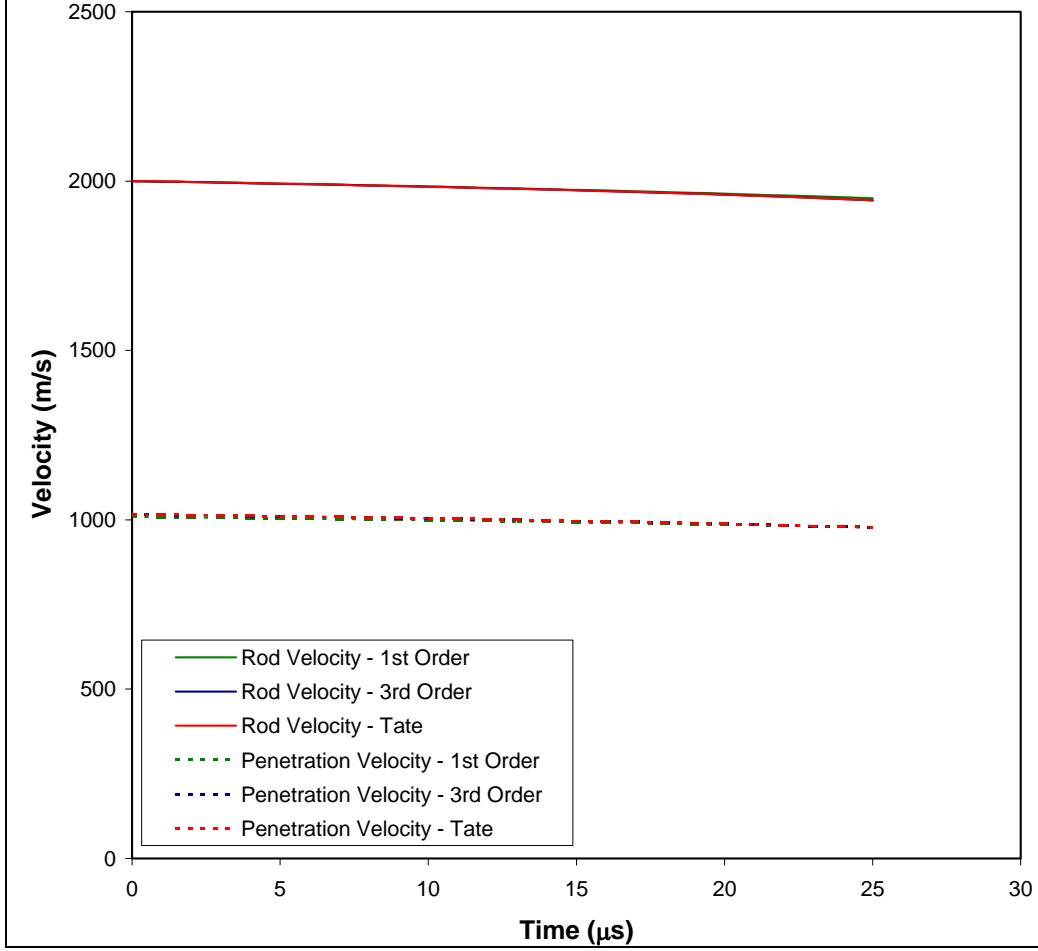


Figure 4. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a 25-mm-thick steel target at an impact velocity of 2000 m/s. The initial rod length was 0.03912 m.

$$\frac{dV}{d\tau} = -\frac{\varepsilon}{\lambda} \left(\frac{1+\mu}{\mu} \right) \left(\frac{Y_p}{R_T} \right), \quad (35)$$

and

$$\frac{d\lambda}{d\tau} = \left(\frac{1+\mu}{\mu} \right) (U - V). \quad (36)$$

This is very similar to the previous set of equations and thus follows the same solution scheme.

Note that the normalization scheme was initiated by dividing the first equation by ρ_p and defining μ^2 to be ρ_T/ρ_p . Alternately, one could divide the equation by ρ_T and define μ^2 to be ρ_p/ρ_T .

Other normalization schemes are possible namely if the nondimensional variables are defined as

$$\lambda = l/L, \quad \mu = \rho_T/\rho_p, \quad K = \frac{Y_p}{\rho_p}, \quad \Sigma = \frac{2(R_T - Y_p)}{\rho_p}, \quad (37)$$

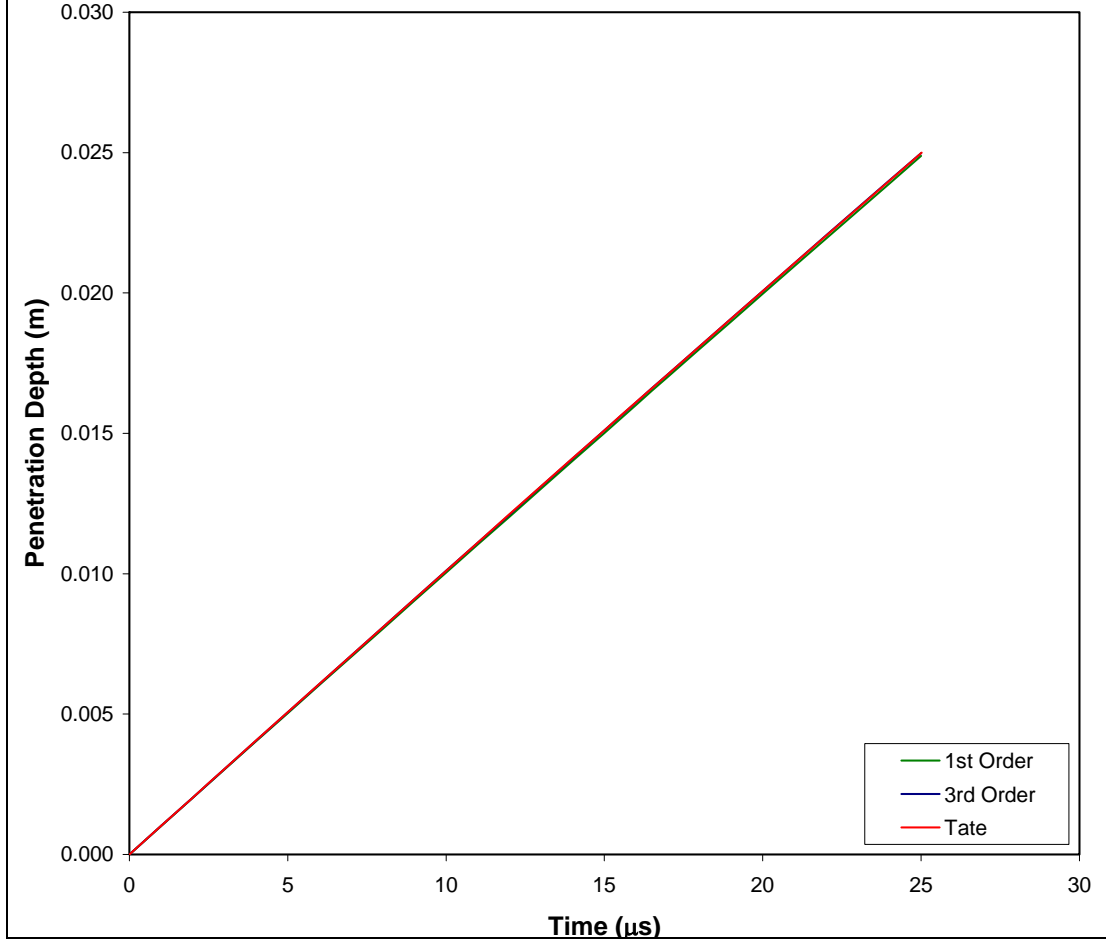


Figure 5. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a 25-mm-thick steel target at an impact velocity of 2000 m/s. The initial rod length was 0.03912 m.

$$V = v/\sqrt{\Sigma}, \quad U = u/\sqrt{\Sigma}, \quad \lambda = l/\sqrt{\Sigma}, \quad \tau = t\sqrt{\Sigma}/L, \quad P = p/L. \quad (38)$$

Note that $\Sigma > 0$ is required. Based on input, if this is not the case, one may reformulate Σ as $\frac{2(Y_p - R_T)}{\rho_T}$.

The equation set becomes

$$(U - V)^2 = \mu U^2 + 1, \quad (39)$$

$$\frac{d\lambda}{d\tau} = U - V, \text{ and} \quad (40)$$

$$\frac{\lambda dV}{d\tau} = \frac{-K}{\Sigma} = \frac{-Y_p}{2(R_T - Y_p)} \quad \text{or} \quad \frac{dV}{d\tau} = \frac{\varepsilon}{\lambda}, \quad (41)$$

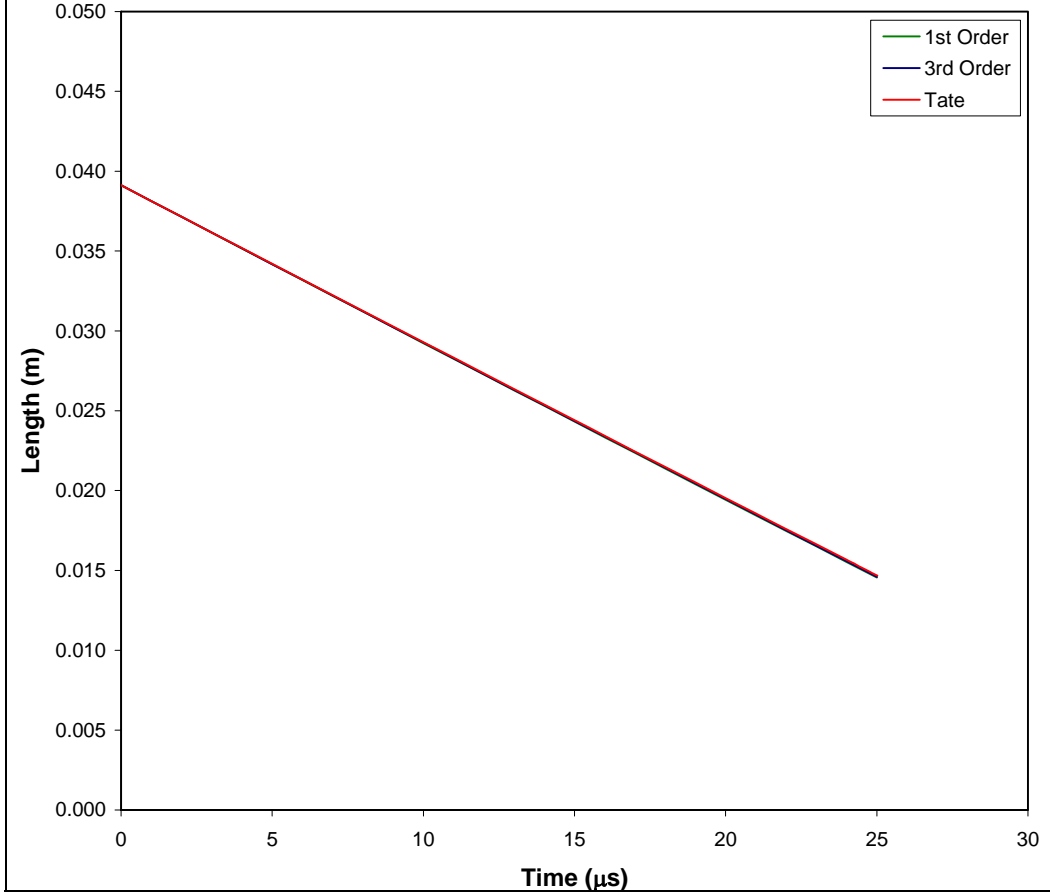


Figure 6. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a 25-mm-thick steel target at an impact velocity of 2000 m/s. The initial rod length was 0.03912 m.

where $\varepsilon = \frac{-K}{\Sigma} = \frac{-Y_p}{2(R_T - Y_p)}$ is chosen to be the perturbation parameter. Again, the previous set of equations is very similar to the original set of equations and thus follows the same solution scheme. The normalization scheme or equation set chosen will depend on the input conditions (known initial values) and the requirement to keep $\varepsilon \ll 1$. Also, it is advantageous to make the time where the logarithmic singularity occurs ($\tau = 1$) as large as possible.

2. Parametric Studies

Other rod-target configurations were studied using the third-order perturbation theory in order to exercise the model. In figure 7, the rod velocity and penetration velocity are plotted vs. time for the Tate solution, the first-order, and the third-order perturbation theory. In this case, the initial rod velocity was 3 km/s. The agreement between the third-order perturbation model and the

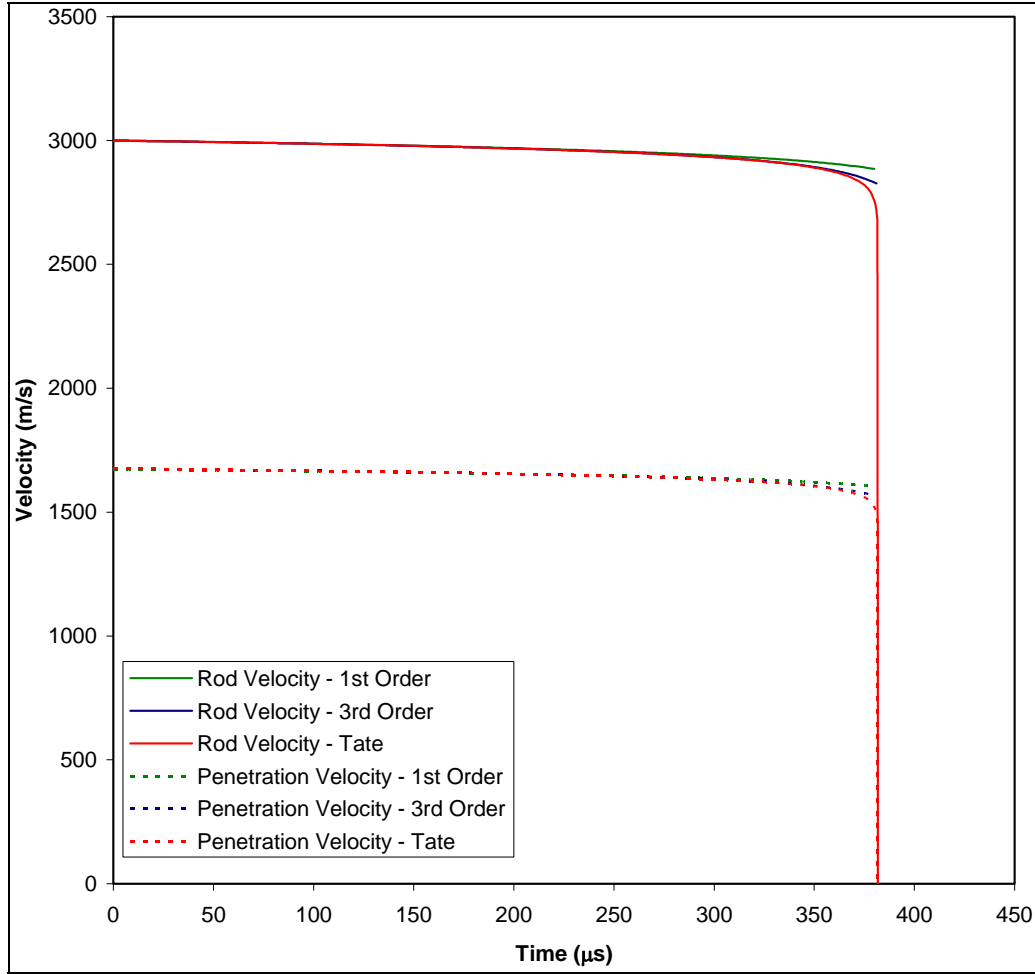


Figure 7. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

Tate solution is excellent, due to the perturbation parameter $\epsilon = 0.0063$, being small. The length and penetration are also in excellent agreement, as shown in figures 8 and 9. The input, namely the strength terms, was obtained from Dr. Steven Segletes of ARL for the tungsten rod vs. the RHA target.

Next, figures 10–12 plot the velocities, penetration, and rod length vs. time for the case studied by Forrestal et al. (4), namely a steel rod impacting a geological (silica-sand) target. The first-order solution, third-order solution, and the Tate solution are compared. The perturbation parameter was 0.0192 and the improvement of the third-order solution over the first-order solution is shown. The Tate solution completes the penetration process at 56 μs . The first-order solution agrees, within 1%, up to 29 μs , which is the Forrestal et al. (4) solution. The third-order solution is valid, again within 1%, to 35 μs .

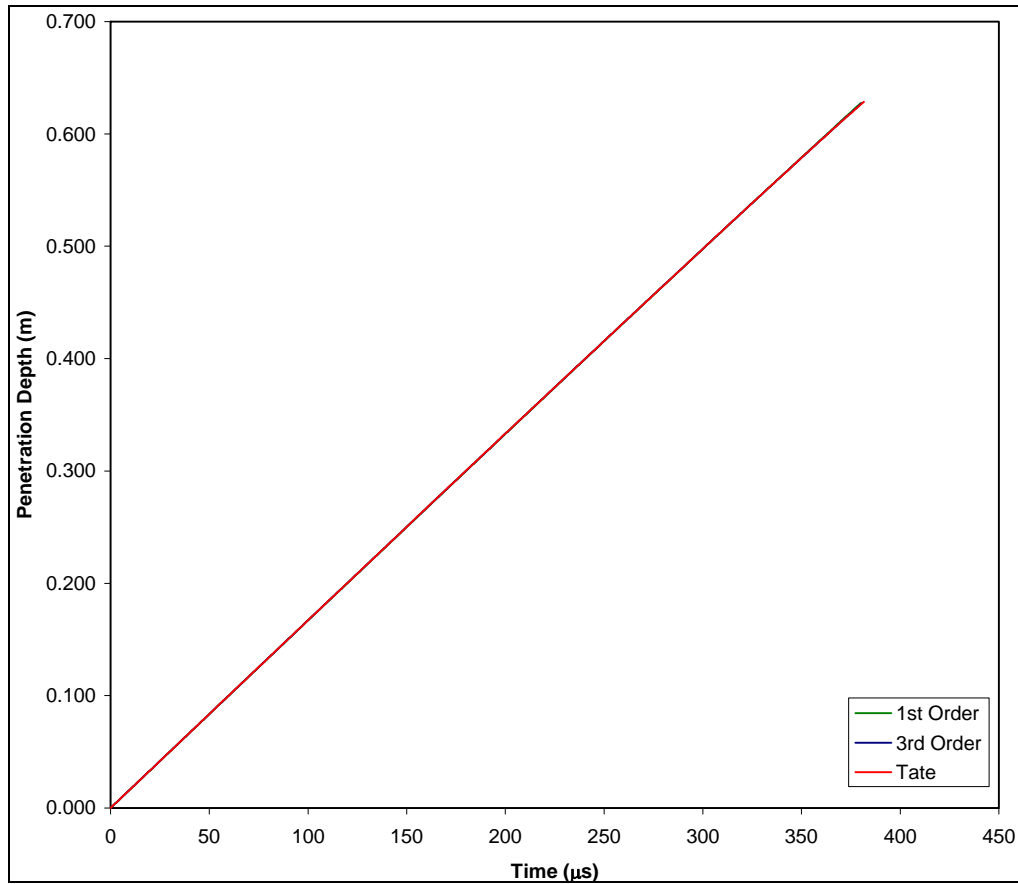


Figure 8. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

As mentioned previously, the strength terms for the steel targets were obtained from Dr. Segletes. Input values used by Edward Horwath of ARL were penetrator strengths of 3.6 GPa for tungsten, 3.2 GPa for depleted uranium (DU), and the target resistance was 5.1 GPa for RHA. All input values used in this study are recorded in table 1. These tungsten values, and the value previously given for the RHA target, are designated as 93% tungsten (the only difference in the two tungstens is the value assigned to Y_p) and the plots are shown in figures 13–15 for an initial rod velocity of 2 km/s. Again, the agreement is good. The Tate solution indicates that the penetration process is complete at 652 μ s and the third-order solution is valid up to 598 μ s. Figures 16–18 present the same plots for an initial impact velocity of 3 km/s. In this case, again because of the lower value of the perturbation parameter, the agreement is excellent. The Tate solution terminates at 428 μ s and the third-order theory is valid up to 409 μ s. The perturbation parameter was 0.0511 for the 2 km/s case and 0.0227 for the 3 km/s case. Table 2 lists the perturbation parameters for all cases. Finally, figures 19–21 give the plots for an initial velocity of 2 km/s for a DU rod impacting RHA. The agreement is good, with the Tate solution terminating at 640.5 μ s and the third-order solution valid up to 611 μ s. The agreement is perfect for the same rod/target configuration at an initial impact velocity of 3 km/s, see figures 22–24.

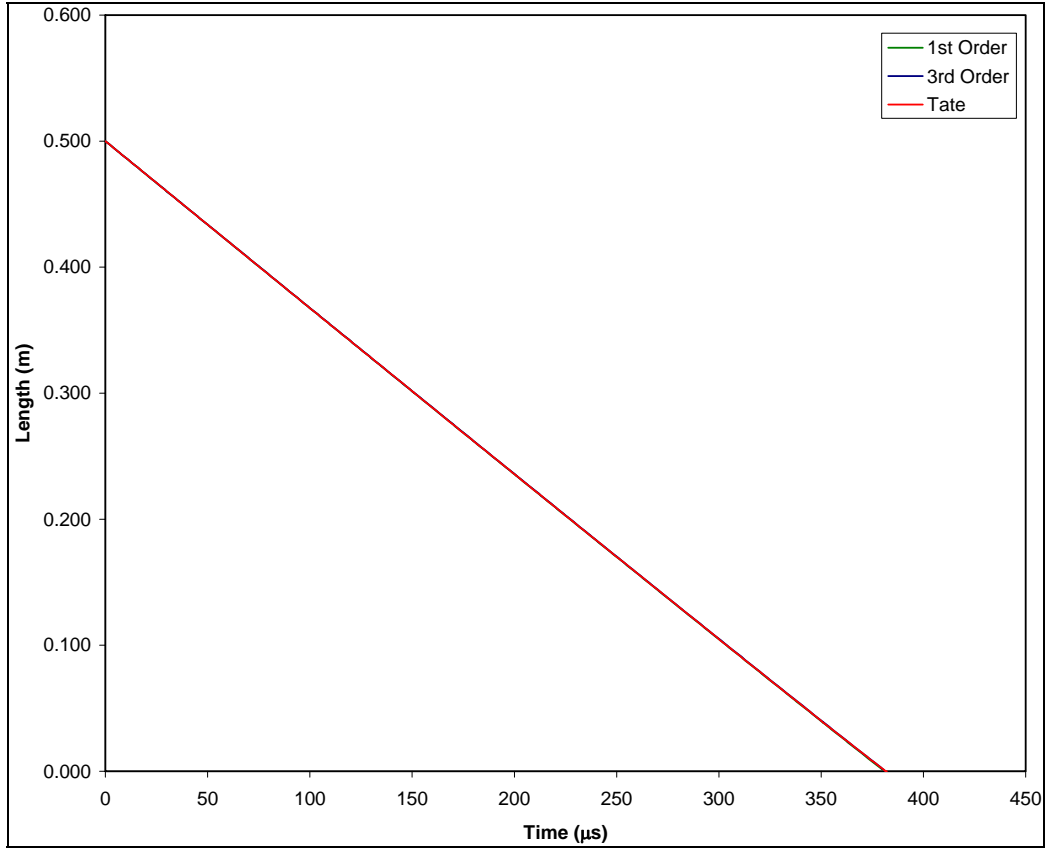


Figure 9. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a tungsten rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

Here, the perturbation parameter was 0.0430 for the 2 km/s case and 0.0191 for the 3 km/s case. All input and perturbation values are summarized in tables 1 and 2.

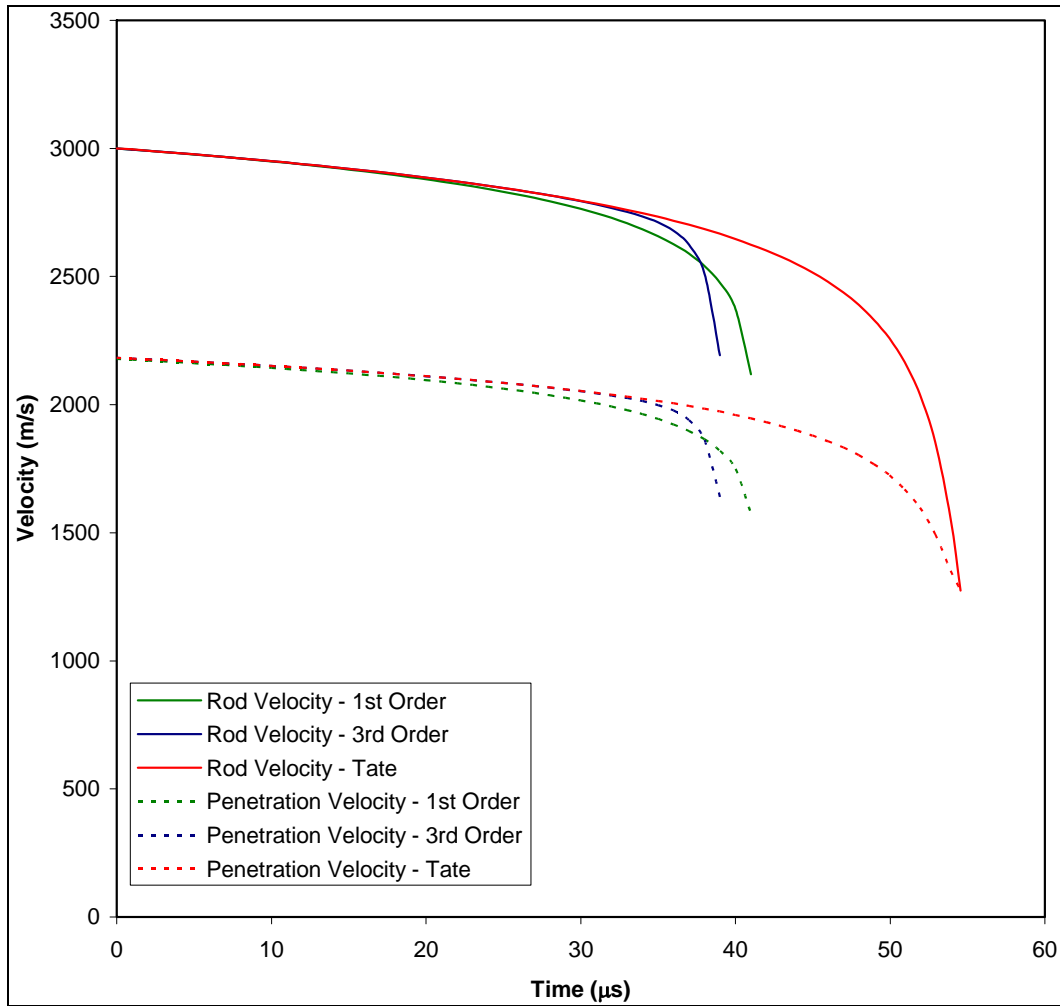


Figure 10. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a steel rod impacting a silica-sand target at an impact velocity of 3000 m/s. The initial rod length was 0.03912 m.

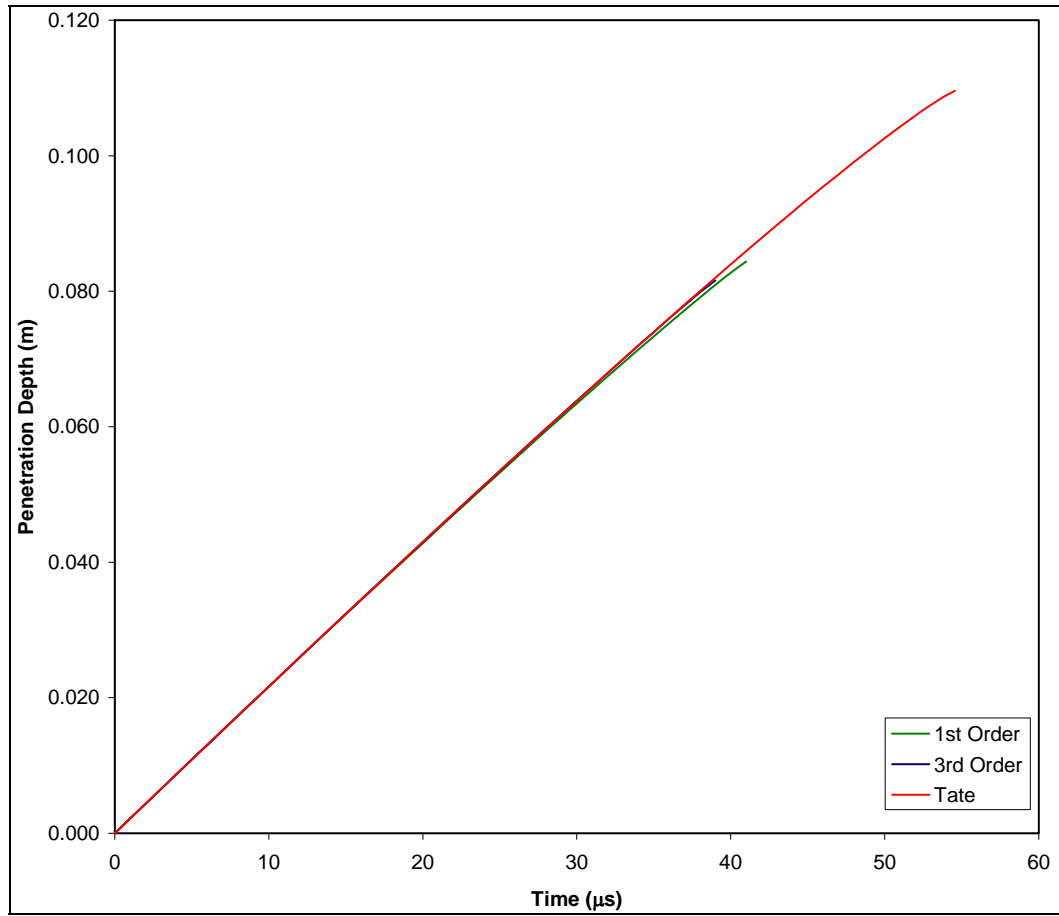


Figure 11. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a steel rod impacting a silica-sand target at an impact velocity of 3000 m/s. The initial rod length was 0.03912 m.

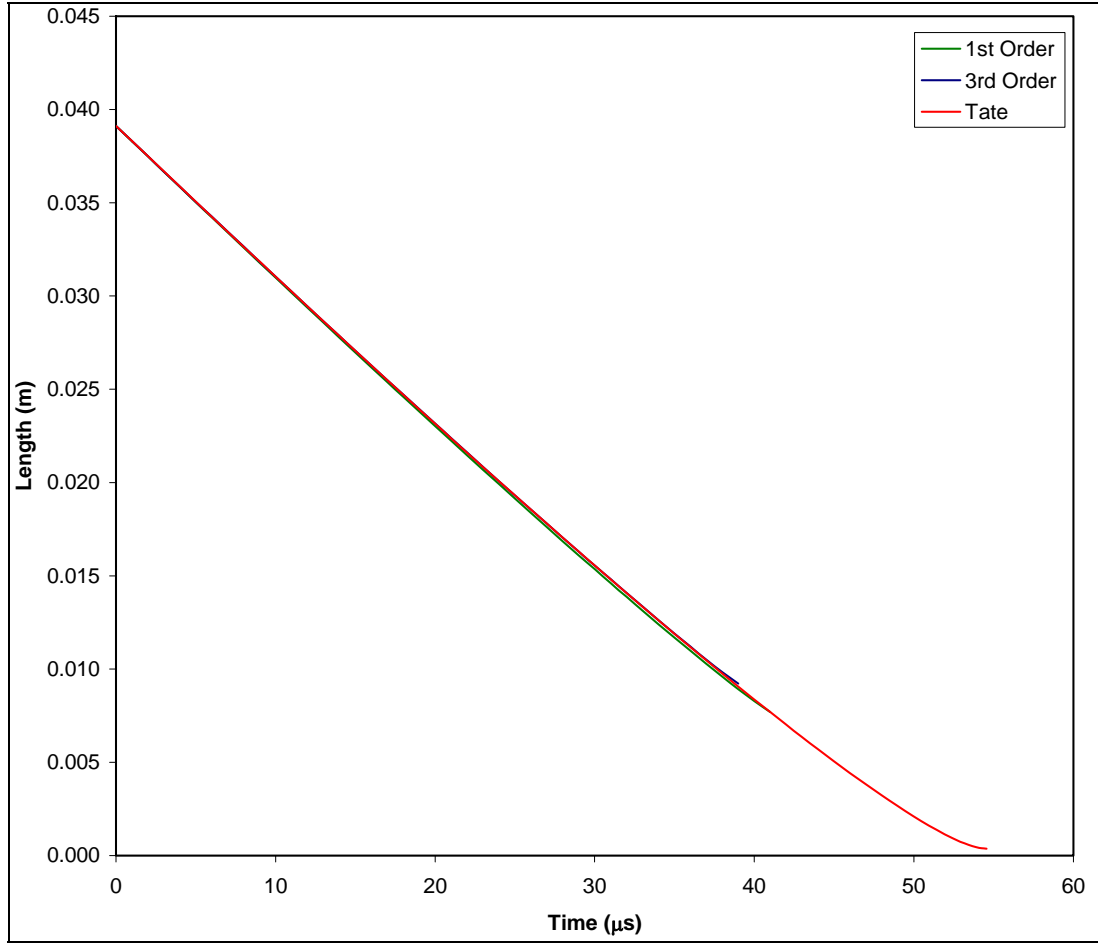


Figure 12. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a steel rod impacting a silica-sand target at an impact velocity of 3000 m/s. The initial rod length was 0.03912 m.

Table 1. Material input properties.

Material	ρ_P (kg/m ³)	ρ_T (kg/m ³)	Y_P (GPa)	R_T (GPa)
Tungsten	17600	—	1.000	—
93% tungsten	17600	—	3.600	—
Depleted uranium (DU)	18600	—	3.200	—
Steel (RHA)	—	7800	—	5.500
Steel (RHA) for 93% tungsten	—	7800	—	5.100
Forrestal penetrator (steel)	8000	—	1.380	—
Forrestal target (silica-sand)	—	1700	—	0.000

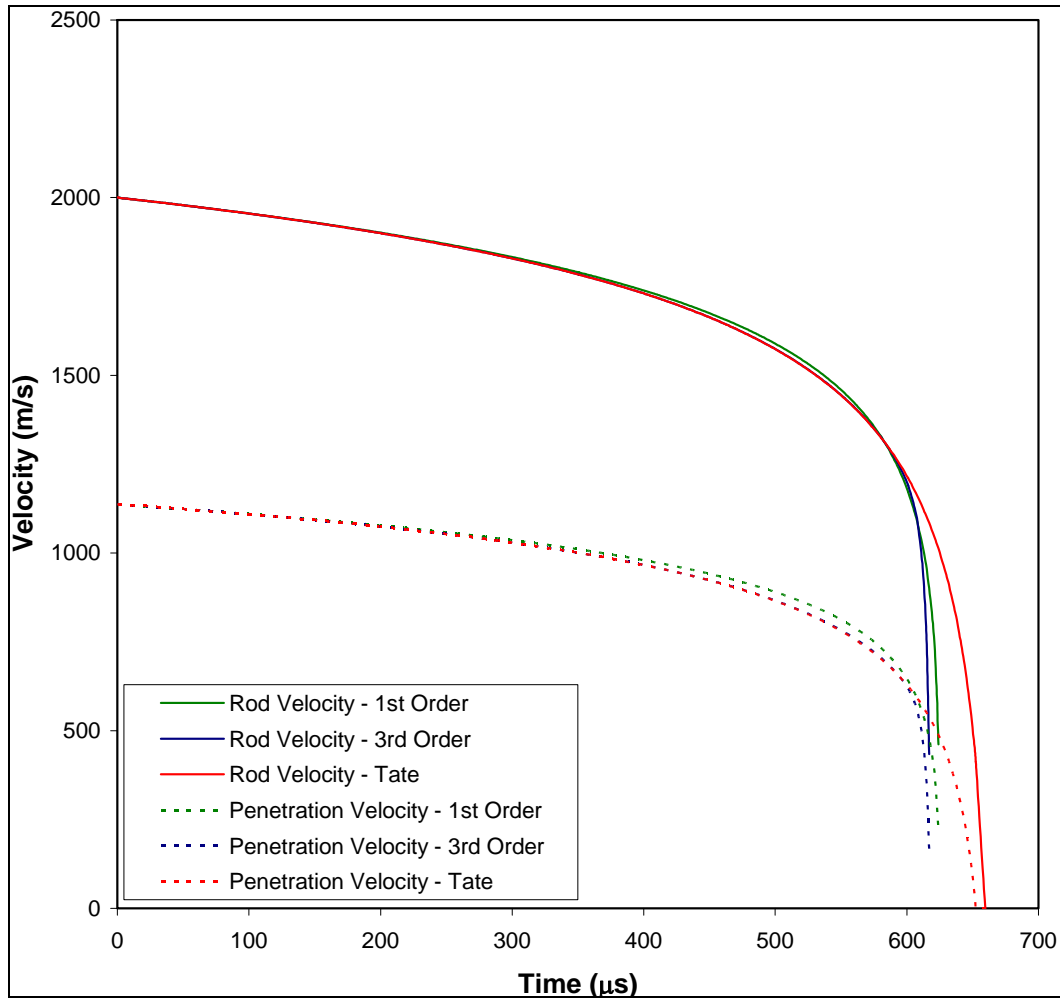


Figure 13. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a 93% tungsten rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

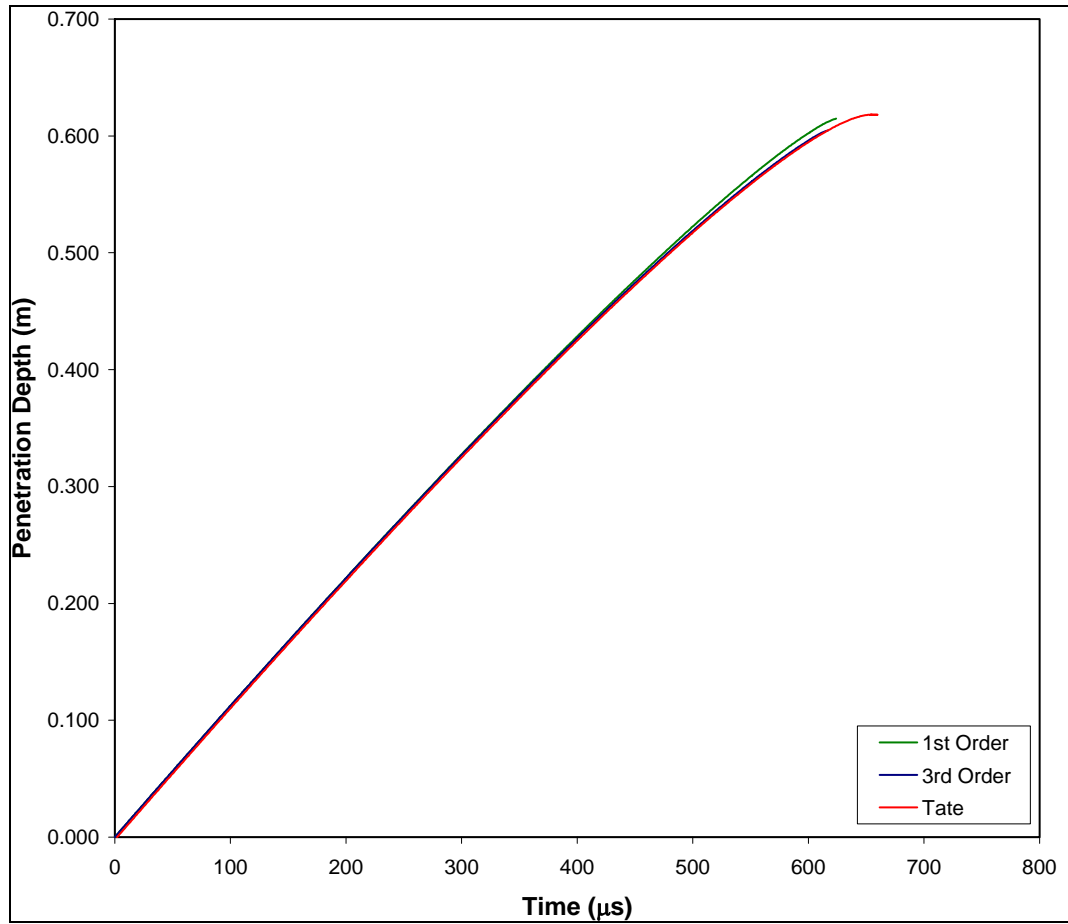


Figure 14. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a 93% tungsten rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

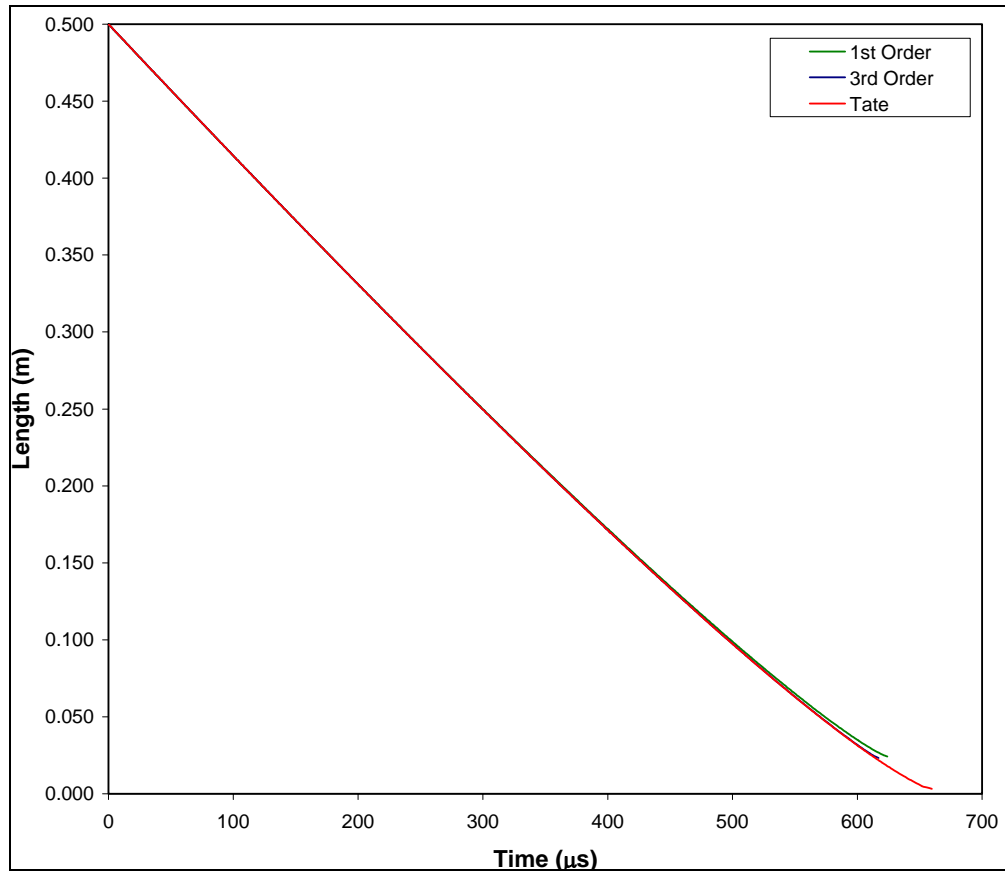


Figure 15. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a 93% tungsten rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

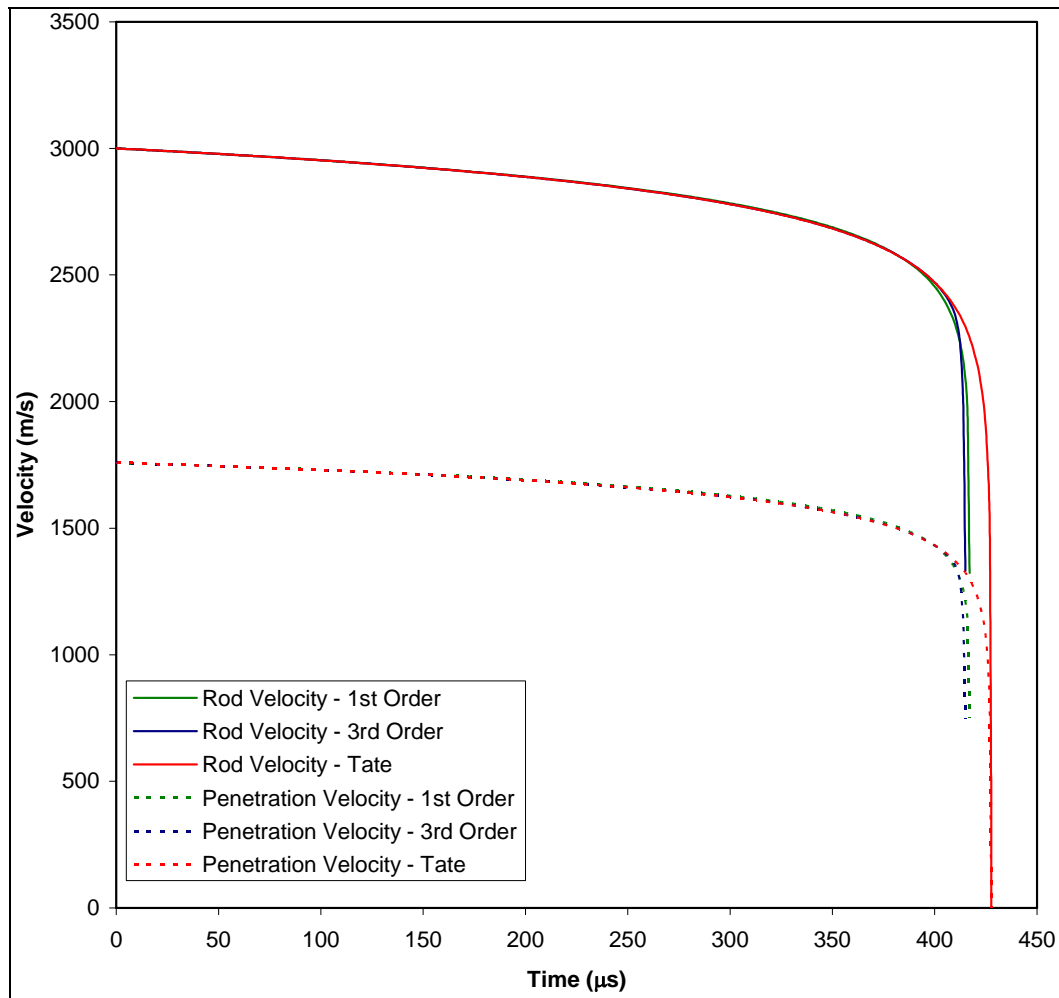


Figure 16. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a 93% tungsten rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

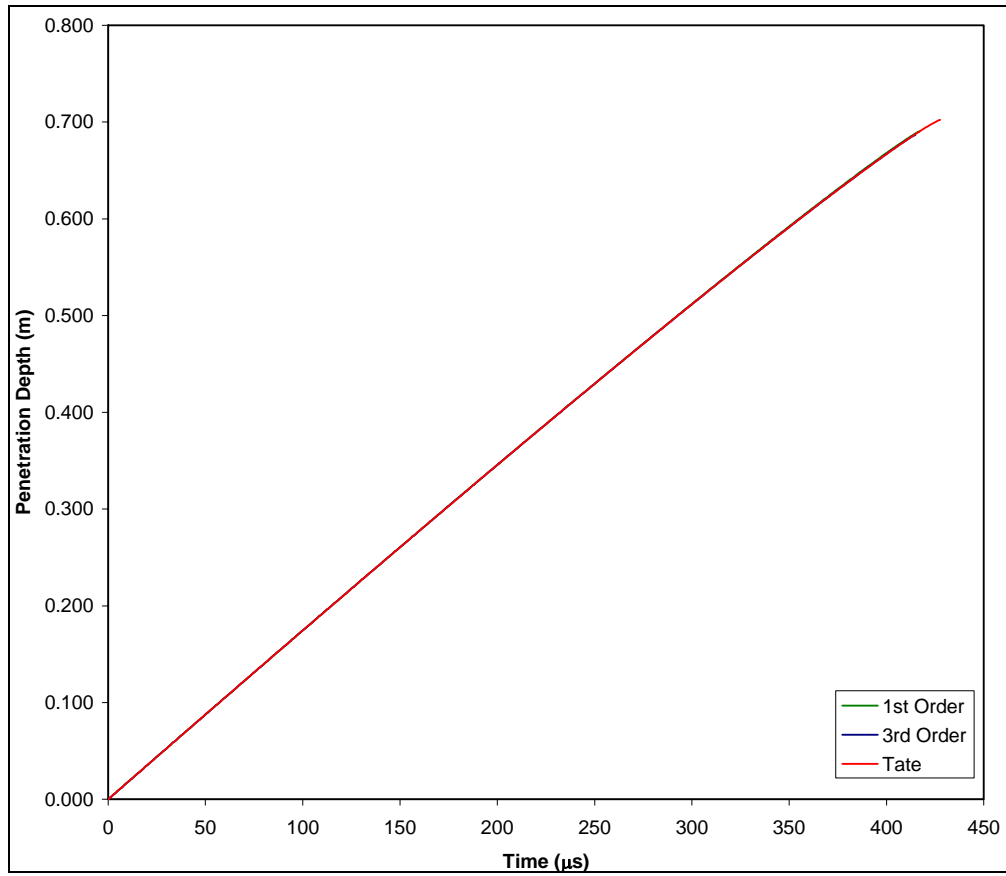


Figure 17. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a 93% tungsten rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

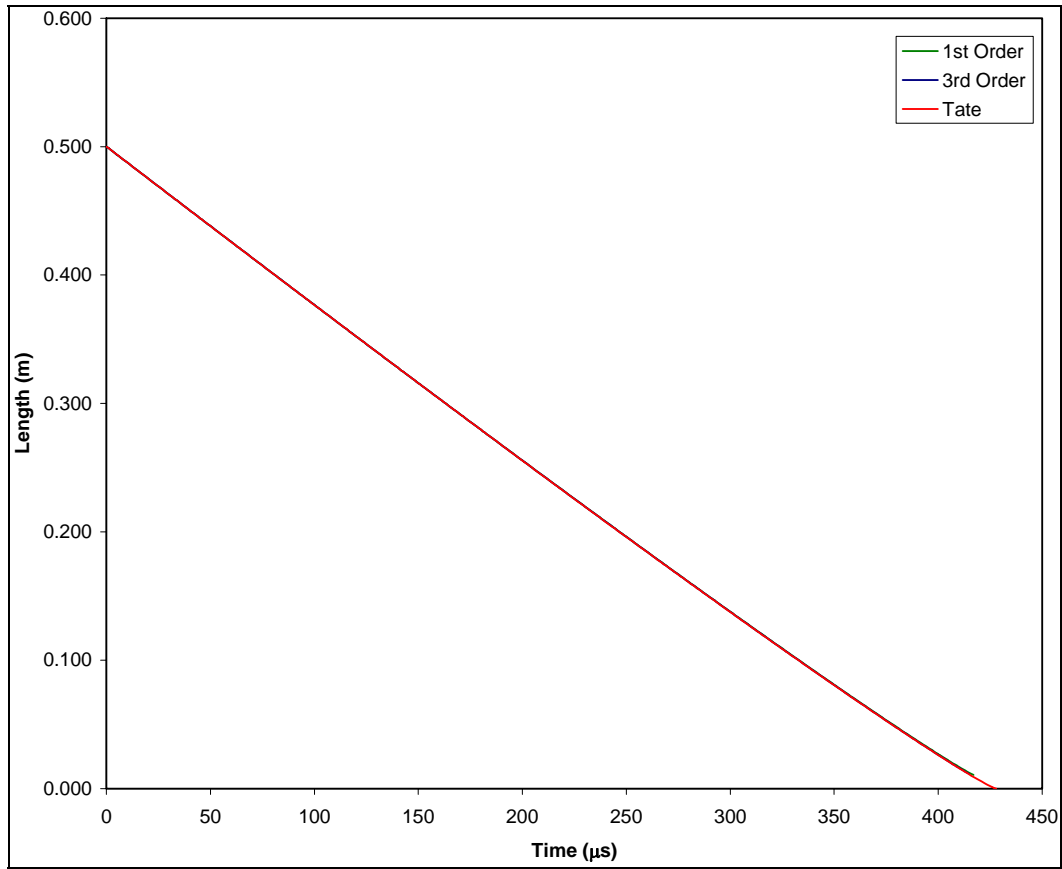


Figure 18. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a 93% tungsten rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

Table 2. Initial values and perturbation parameters.

Penetrator	Target	L_o (m)	V_i (m/s)	ϵ
Tungsten	Steel (RHA)	0.500	2000	0.0140
Tungsten	Steel (RHA)	0.500	3000	0.0063
93% tungsten	Steel (RHA)	0.500	2000	0.0511
93% tungsten	Steel (RHA)	0.500	3000	0.0227
Depleted uranium (DU)	Steel (RHA)	0.500	2000	0.0430
Depleted uranium (DU)	Steel (RHA)	0.500	3000	0.0191
Forrestal steel	Silica-sand	0.039	3000	0.0192

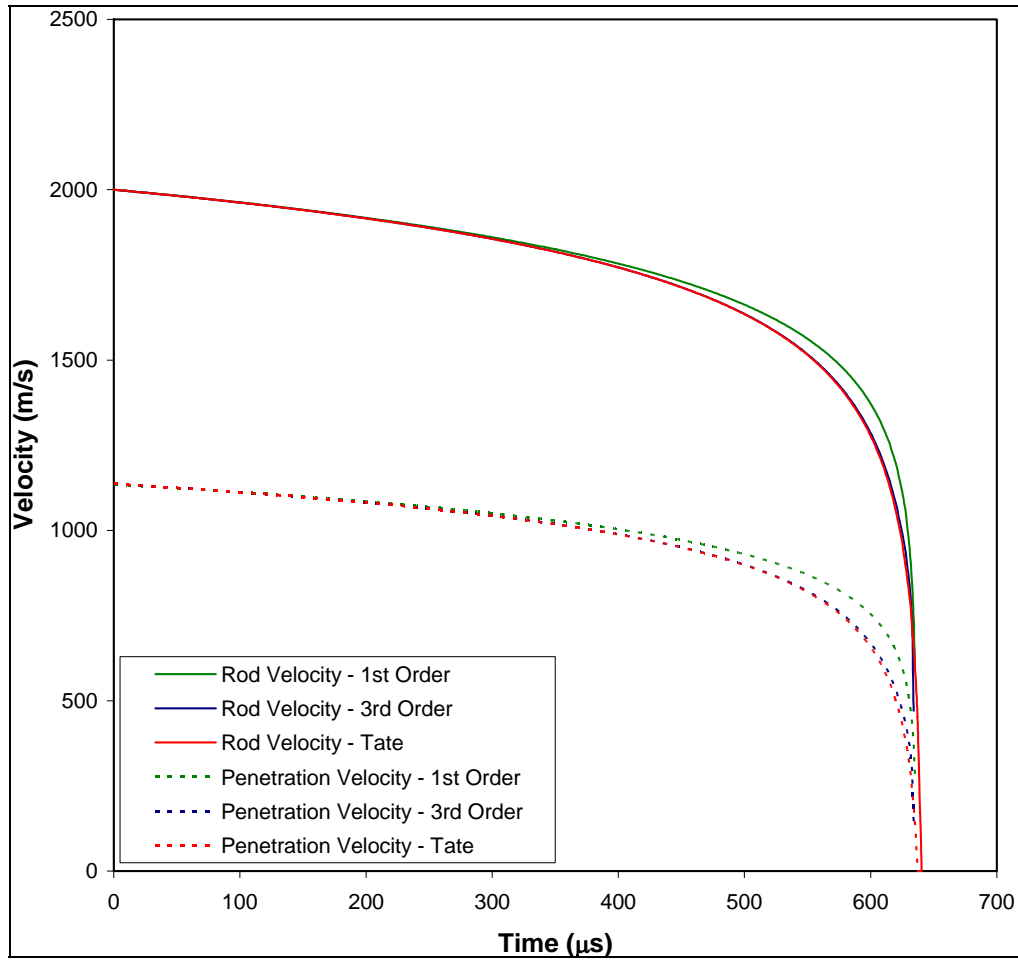


Figure 19. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a depleted uranium rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

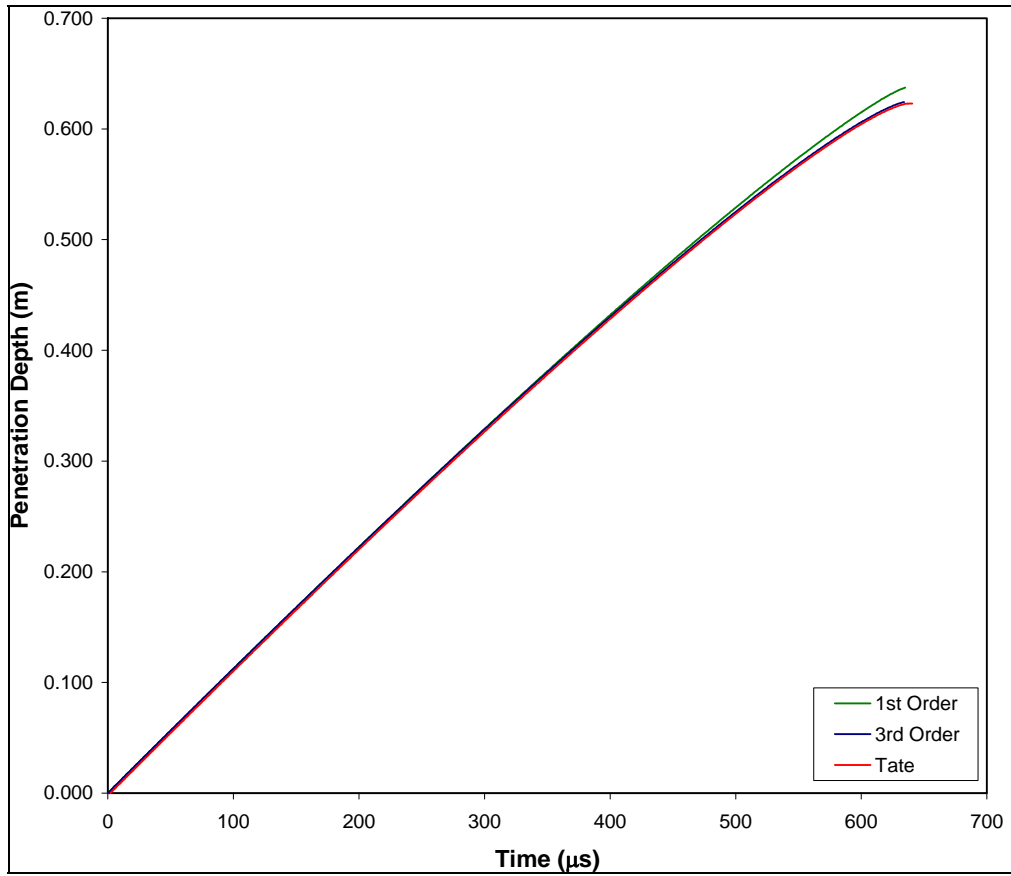


Figure 20. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a depleted uranium rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

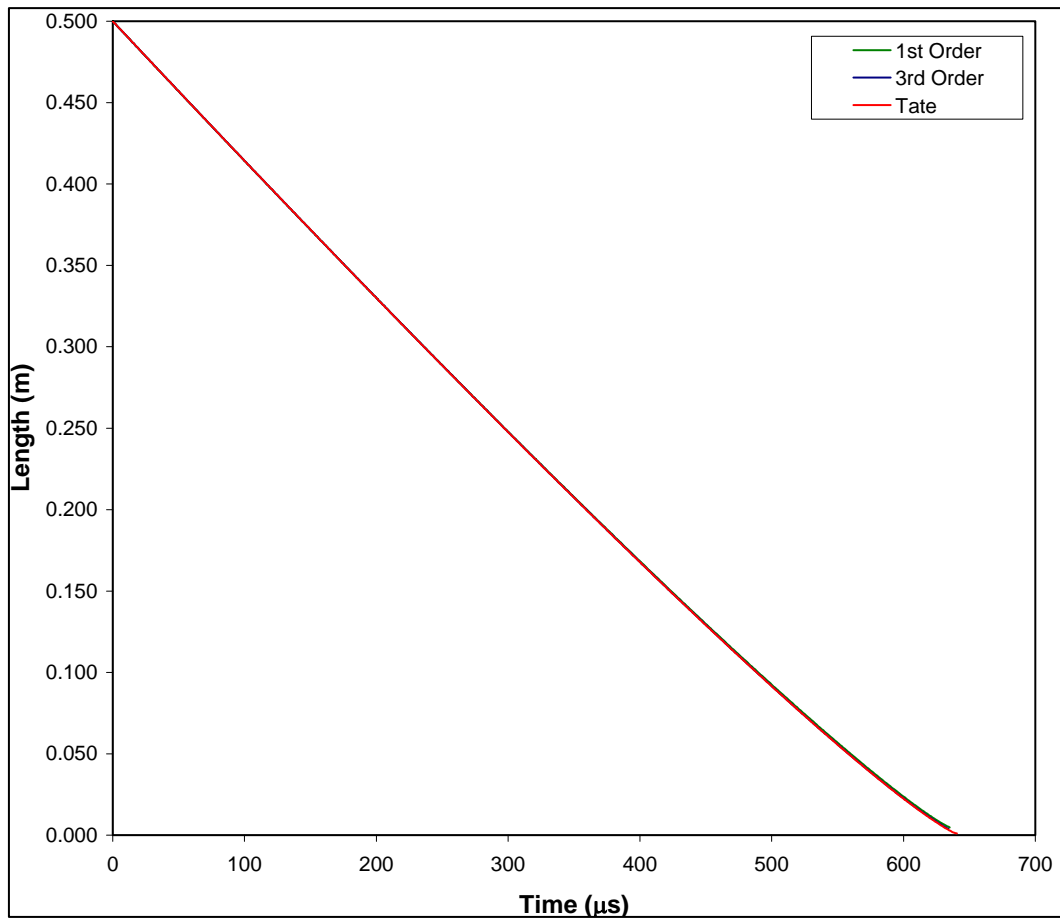


Figure 21. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a depleted uranium rod impacting a steel target at an impact velocity of 2000 m/s. The initial rod length was 0.500 m.

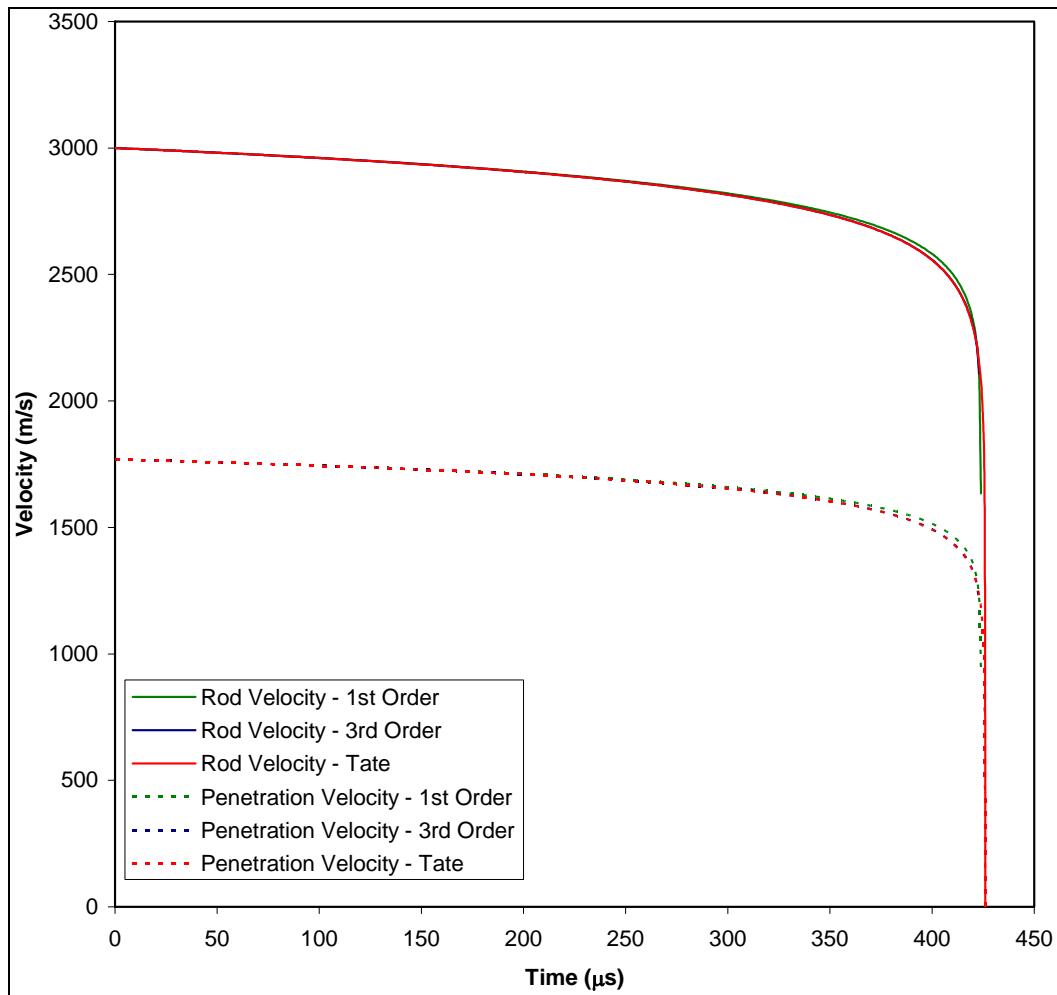


Figure 22. Comparison between rod and penetration velocities for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a depleted uranium rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

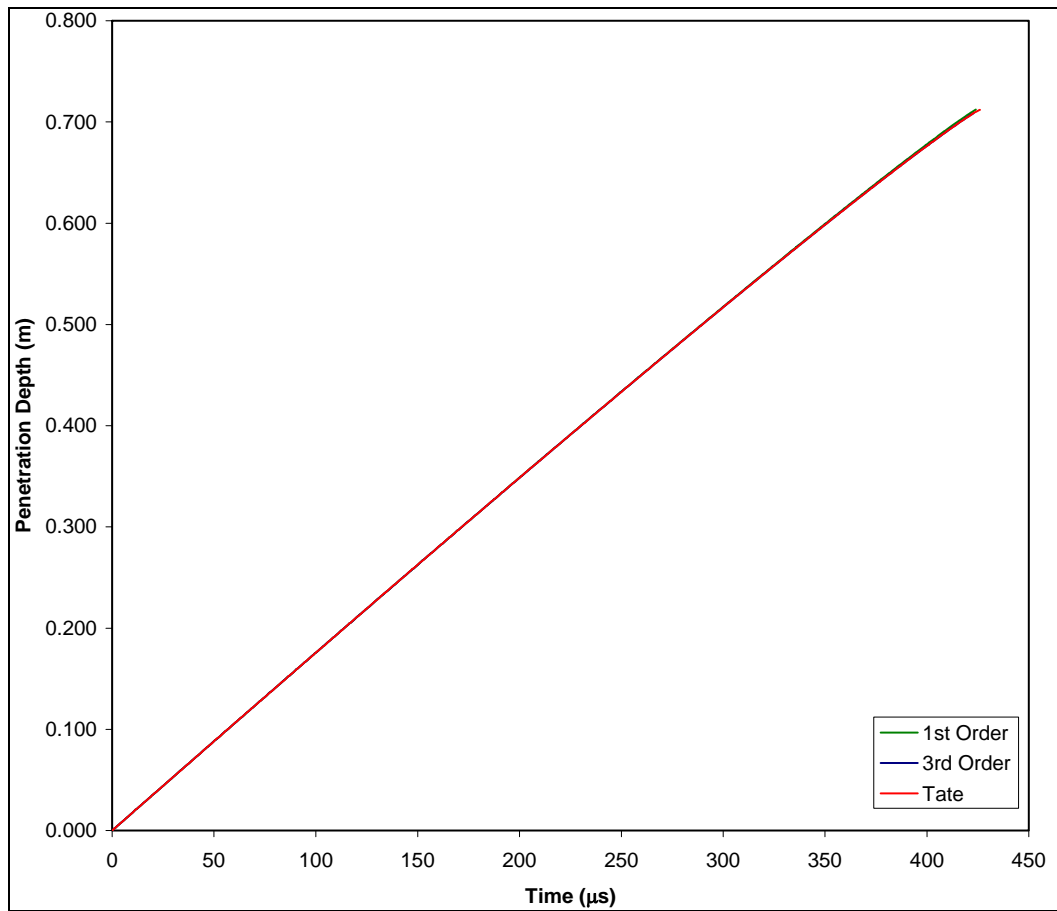


Figure 23. Penetration depth for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a depleted uranium rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

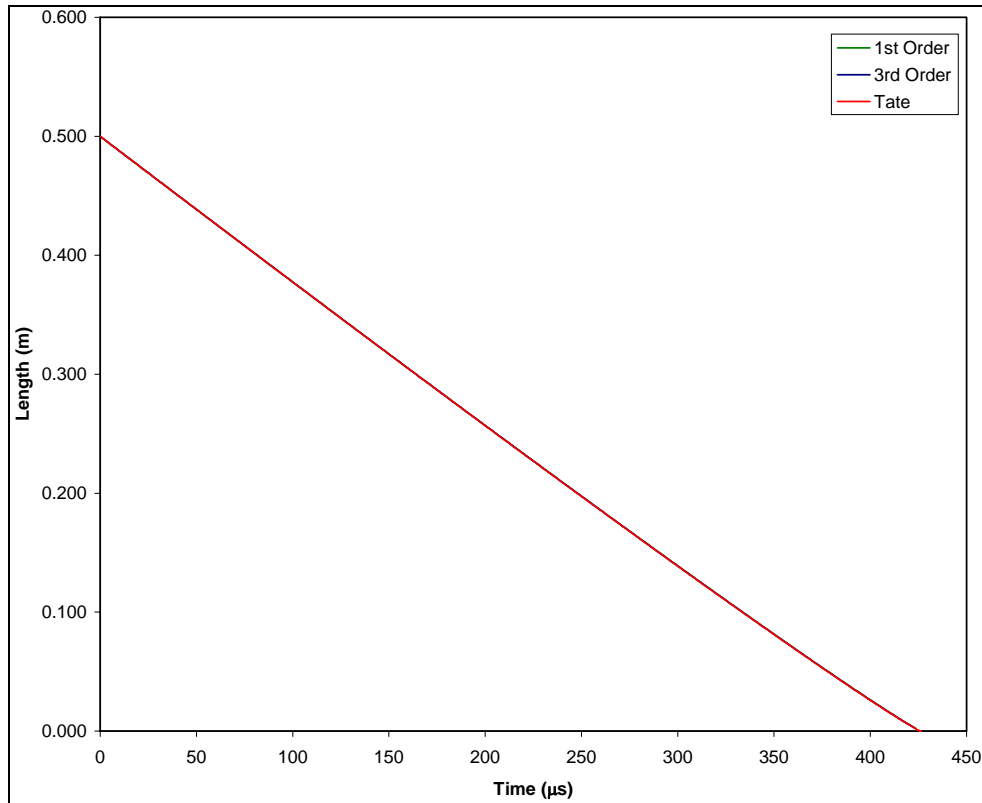


Figure 24. Rod length for a first-order perturbation solution, a third-order perturbation solution, and the exact Tate solution. This case is for a depleted uranium rod impacting a steel target at an impact velocity of 3000 m/s. The initial rod length was 0.500 m.

3. Conclusions

A perturbation solution of the Alekseevski-Tate equations was obtained through the third order. Agreement with the exact solution is excellent for a tungsten rod impacting a steel target at a velocity of 2.0 km/s, as well as for other cases of interest to ballisticians involved in the penetration of steel targets. Also, the velocities and residual length of a tungsten rod perforating a finite-thickness steel plate show excellent agreement with the exact equations. The approximate (perturbation) solution yields the dependent variables (V , U , λ , and P) as explicit functions of time. Also, alternate forms of the normalization of the pertinent equations are investigated to obtain a perturbation parameter much less than one for various penetration problems depending on the input conditions, namely target and penetrator densities, strengths, and initial impact conditions. Also, comments are made regarding the singularity in time. Extensions of the method to higher orders (i.e., the fourth order) are possible, but a point of diminishing returns has been reached. The current third-order solution is expressible as an algebraic equation, amenable to a spread sheet or simple calculator evaluation.

4. References

1. Tate, A. A Theory for the Deceleration of Long Rods after Impact. *J. Mech. Phys. Solids* **1967**, *15*, 387–399.
2. Walters, W. P.; Segletes, S. B. An Exact Solution of the Long Rod Penetration Equations. *International Journal of Impact Engineering* **1991**, *11* (2), 225–231.
3. Segletes, S. B.; Walters, W. P. Extensions to the Exact Solution of the Long-Rod Penetration/Erosion Equations. *International Journal of Impact Engineering* **2003**, *11*, 363–376.
4. Forrestal, M. J.; Piekutowski, A. J.; Luk, V. K. Long-Rod Penetration into Simulated Geological Targets at an Impact Velocity of 3.0 km/s. Presented at the *11th International Symposium on Ballistics*, Brussels, Belgium, 9–11 May 1989, Vol. 2.
5. Cole, J. D. *Perturbation Methods in Applied Mathematics*. Blaisdell Publishing Company: Waltham, MA, 1968.

Appendix. FORTRAN Computer Program

```
! Pertubation.f90
!
! FUNCTIONS:
! Pertubation - Closed-form equations for Tate's model from a pertubation analysis.
!
!*****!
! PROGRAM: Pertubation
!
! PURPOSE: This program calculates the rod velocity, penetration velocity, penetration
!          depth, and instantaneous length using pertubation method up to the third-order
!          correction terms.
!*****

program Pertubation

implicit none

! Identifiers
!   RT: Strength resistance of target (Kg/m.s^2)
!   RHO_P: Density of penetrator (Kg/m^3)
!   RHO_T: Density of target (Kg/m^3)
!   YP: Flow stress of penetrator (Pa)
!   VI: Impact velocity (m/s)
!   VR: Rod velocity (m/s)
!   UP: Penetration velocity (m/s)
!   LO: Original length of penetrator (m)
!   LI: Instantaneous length of rod (m)
!   P: Penetration Depth (m)
!   T: Time (microsecond)
!   VN: Normalized rod velocity
!   UN: Normalized penetration velocity
!   PD: Normalized penetration depth
!   LAMDA: Normalized length
!   TAU: Normalized time
!   MHU: Dimensionless variable
!   BETA: Dimensionless variable
!   ALPHA: Dimensionless variable
!   EPSI: Dimensionless variable
!   A,B: Expressions used for equation compactness

DOUBLEPRECISION RT, RHO_P, RHO_T, YP, VI, VR, UP, LO, LI, P, PD, T, VN, UN, LAMDA, TAU,
MHU, BETA, ALPHA, EPSI, V0, U0, LAMDA0, PD0, V1, U1, LAMDA1, PD1, V2, U2, LAMDA2, PD2, V, U,
C0, C1, C2, C3, V3, U3, PD3, LAMDA3, THK, A, B

INTEGER:: ORDER

! Input values for velocity, length, and material constants
```

```

PRINT*, "Enter impact velocity of penetrator, 'Meters per Second'"
READ*, VI

PRINT*, "Enter original length of penetrator, 'Meters'"
READ*, LO

PRINT*, "Enter density of penetrator material, 'Kilograms per Meter Cubed'"
READ*, RHO_P

PRINT*, "Enter density of target material, 'Kilograms per Meter Cubed'"
READ*, RHO_T

PRINT*, "Enter flow stress of penetrator material, 'Pascals'"
READ*, YP

PRINT*, "Strength resistance of target, 'Pascals'"
READ*, RT

!      Check for data inconsistencies
!      The "strength resistance of the target (RT)," cannot be equal to the "flow stress of the
!      penetrator (YP)," for the perturbation solution to be meaningful.

IF(RT.EQ.YP)THEN

PRINT*, "*****RT must not equal YP for a meaningful perturbation solution.*****"

STOP

ENDIF

PRINT*, "Thickness of the target, 'Meters'"

READ*, THK

!      Assume a semi-infinite plate for zero thickness.

IF(THK.EQ.0)THEN
    THK=1
ENDIF

PRINT*, "What order perturbation solution do you require"

READ*, ORDER

OPEN(UNIT=12, FILE="Perturbation.dat", STATUS="OLD")

!      Normalization scheme

MHU=SQRT(RHO_T/RHO_P)

BETA=MHU/(1.0+MHU)*VI/LO

ALPHA=(RT-YP)/YP

EPSI=YP/(RHO_P*VI**2)

```

```

A=(1.0+MHU)/MHU

B=1.0-ALPHA/MHU

T=0.0

DO

    TAU=BETA*T

! Zero order calculation resulting from pertubation analysis

    V0=1.0

    U0=1.0/(1.0+MHU)

    LAMDA0=1.0-TAU

    PD0=TAU/MHU

! First order calculation resulting from pertubation analysis

    V1=((1.0+MHU)/MHU)*LOG(1.0-TAU)

    U1=(1.0/MHU)*(LOG(1.0-TAU)-ALPHA)

    LAMDA1=((1.0+MHU)/MHU)*((1.0-ALPHA/MHU)*TAU+(1.0-TAU)*LOG(1.0-TAU))

    PD1=-((1.0+MHU)/(MHU**2))*(TAU*(ALPHA+1.0)+(1.0-TAU)*LOG(1.0-TAU))

! Second order calculation resulting from pertubation analysis

    V2=((1.0+MHU)/MHU)**2*(1.0-ALPHA/MHU)*(LOG(1.0-TAU)+1/(1.0-TAU)-1.0)- &
    0.5*(((1.0+MHU)/MHU)**2)*(LOG(1.0-TAU))**2

    U2=V2/(1.0+MHU)+(ALPHA/MHU**2)*(1.0+MHU)*LOG(1.0-TAU)+(ALPHA**2)*(1.0-&
    MHU**2)/(2.0*MHU**3)

    C0=3.0-3.0*ALPHA/MHU+ALPHA**2/(2.0*MHU**2)-ALPHA**2/(2.0*MHU)

    LAMDA2=((1.0+MHU)/MHU)**2*(-(3.0-3.0*ALPHA/MHU+ALPHA**2/(2.0*MHU**2))-&
    ALPHA**2/(2.0*MHU))*(1-TAU)+(1.0-ALPHA/MHU)*LOG(1.0-TAU)+2.0*(1.0-&
    ALPHA/MHU)*(1.0-TAU)*LOG(1.0-TAU)-0.5*(1.0-TAU)* (LOG(1.0-TAU))**2+C0)

    PD2=((1.0+MHU)**2/MHU**3*(B*(1.0-2.0*TAU-(1.0-TAU)*LOG(1.0-TAU)-LOG(1.0-&
    TAU))/2.0*(LOG(1.0-TAU))**2-(1.0-TAU)*LOG(1.0-TAU)+1.0-&
    TAU+ALPHA*(1.0-TAU-(1.0-TAU)*LOG(1.0-TAU))+ ALPHA**2*(1.0-&
    MHU)*TAU/(2.0*MHU)-(2+ALPHA-ALPHA/MHU))

! Third order calculation resulting from pertubation analysis

    C1= -3.0/2.0*B**2-2.0*B+ALPHA**2/(2.0*MHU)*(1.0-1.0/MHU)

    V3=A**3*((4.0-5.0*ALPHA/MHU-ALPHA**2/(2.0*MHU)+3.0*ALPHA**2/(2.0*MHU**2))&
    *LOG(1.0-TAU)-0.5*B**2*1.0/(1.0-TAU)**2+(2.0*B+2.0*B**2-ALPHA**2/(2.0*MHU)+ &

```

$$\text{ALPHA}^{**2}/(2.0*\text{MHU}^{**2}))*1.0/(1.0-\text{TAU})-2.0*B*(\text{LOG}(1.0-\text{TAU}))^{**2}+0.5*(\text{LOG}(1.0-\&\text{TAU}))^{**3}-B*(\text{LOG}(1.0-\text{TAU}))/((1.0-\text{TAU})+C1)$$

$$U3=(V3*(V0-U0)+(V1-U1)*(V2-U2)-\text{MHU}^{**2}*U1*U2)/((V0-U0)+U0*\text{MHU}^{**2})$$

$$C2=(1.0+\text{MHU})^{**3}/\text{MHU}^{**4}*(-4.0-7.0/2.0*B^{**2}-7.0*B+9.0/2.0*\text{ALPHA}^{**2}/\text{MHU}-\&5.0*\text{ALPHA}-3.0*\text{ALPHA}^{**2}/2.0-\text{ALPHA}^{**3}/(2.0*\text{MHU}^{**2})*(1.0-\text{MHU})^{**2}+B^{**2}/2.0)$$

$$\begin{aligned} \text{PD3}= & -(1.0+\text{MHU})^{**3}/\text{MHU}^{**4}*((1.0-\text{TAU})*(-4.0-7.0/2.0*B^{**2}-7.0*B+9.0/2.0*\&\text{ALPHA}^{**2}/\text{MHU}- \\ & 5.0*\text{ALPHA}-3.0*\text{ALPHA}^{**2}/2.0-\text{ALPHA}^{**3}* \\ & (1.0-\text{HU})^{**2}/(2.0*\text{MHU}^{**2}))+ (1.0-\text{TAU})*\text{LOG}(1.0-\text{TAU})*(7.0/2.0+6.0*B+\& \\ & +3.0*\text{ALPHA}*B+3.0*B^{**2}/2.0+\text{ALPHA}+3.0*\text{ALPHA}^{**2}/2.0)+B^{**2}/(2.0*(1.0-\text{TAU}))\& \\ & +(B+5.0/2.0*B^{**2}+\text{ALPHA}-3.0*\text{ALPHA}^{**2}/(2.0*\text{MHU})+1.0/2.0)*\text{LOG}(1.0-\text{TAU})+(1.0-\& \\ & \text{TAU})*(\text{LOG}(1.0-\text{TAU}))^{**2}*(-2.0*B-3.0/2.0*(1.0+\text{ALPHA}))-B/2.0*(\text{LOG}(1.0-\text{TAU}))^{**2}+(1.0-\& \\ & \text{TAU})/2.0*(\text{LOG}(1.0-\text{TAU}))^{**3})+C2 \end{aligned}$$

$$C3=((1+\text{MHU})/\text{MHU})^{**3}*(5.0/2.0+13.0/2.0*B^{**2}+5.0*B-5.0*\text{ALPHA}^{**2}/(2.0*\text{MHU})-\&\text{ALPHA}^{**3}/(2.0*\text{MHU}^{**3})*(\text{MHU}-1)^{**2})$$

$$\begin{aligned} \text{LAMDA3}= & ((1+\text{MHU})/\text{MHU})^{**3}*((-7.0*B/2.0)*(1.0-\text{TAU})*(\text{LOG}(1.0-\text{TAU}))^{**2}+(7.0*\&B^{**2}/2.0- \\ & \text{ALPHA}^{**2}/(2.0*\text{MHU})+1.0/2.0)*\text{LOG}(1.0-\text{TAU})-B/2.0*(\text{LOG}(1.0-\text{TAU}))^{**2}\&+(2.0+5.0*B+4*B^{**2}- \\ & 2*\text{ALPHA}^{**2}/\text{MHU})*(1.0-\text{TAU})*\text{LOG}(1.0-\text{TAU})+(-5.0/2.0-7.0*B^{**2}\& \\ & -5.0*B+5.0*\text{ALPHA}^{**2}/(2.0*\text{MHU})+\text{ALPHA}^{**3}/(2.0*\text{MHU}^{**3})*(\text{MHU}-1)^{**2})\& \\ & *(1.0-\text{TAU})+B^{**2}/(2.0*(1.0-\text{TAU}))+ (1.0-\text{TAU})/2.0*(\text{LOG}(1.0-\text{TAU}))^{**3})+C3 \end{aligned}$$

! Summation of series for 1st order, 2nd order, and 3rd order pertubation solution

IF(ORDER.EQ.1)THEN

$$V=V0+\text{EPSI}*V1$$

$$U=U0+\text{EPSI}*U1$$

$$\text{LAMDA}=\text{LAMDA0}+\text{EPSI}*\text{LAMDA1}$$

$$\text{PD}=\text{PD0}+\text{EPSI}*\text{PD1}$$

ELSEIF(ORDER.EQ.2)THEN

$$V=V0+\text{EPSI}*V1+(\text{EPSI}^{**2})*V2$$

$$U=U0+\text{EPSI}*U1+(\text{EPSI}^{**2})*U2$$

$$\text{LAMDA}=\text{LAMDA0}+\text{EPSI}*\text{LAMDA1}+(\text{EPSI}^{**2})*\text{LAMDA2}$$

$$\text{PD}=\text{PD0}+\text{EPSI}*\text{PD1}+(\text{EPSI}^{**2})*\text{PD2}$$

ELSEIF(ORDER.EQ.3)THEN

$$V=V0+\text{EPSI}*V1+(\text{EPSI}^{**2})*V2+(\text{EPSI}^{**3})*V3$$

$$U=U0+\text{EPSI}*U1+(\text{EPSI}^{**2})*U2+(\text{EPSI}^{**3})*U3$$

$$\text{LAMDA}=\text{LAMDA0}+\text{EPSI}*\text{LAMDA1}+(\text{EPSI}^{**2})*\text{LAMDA2}+(\text{EPSI}^{**3})*\text{LAMDA3}$$

```

        PD=PD0+EPSI*PD1+(EPSI**2)*PD2+(EPSI**3)*PD3
    ENDIF

!      Converting normalized values into actual values

        VR=V*VI

        UP=U*VI

        P=PD*LO

        LI=LAMDA*LO

!      Penetration process stop conditions

! For RT > YP, the minimum rod velocity required to achieve penetration occurs when the penetration
! velocity is zero (UP = 0). At this point the target begins to behave as a rigid body and the rod
! bounces off the target.

        IF(RT.GT.YP.AND.VR.LE.SQRT(2.0*(RT-YP)/RHO_P))EXIT

! For RT < YP, the minimum rod velocity required to achieve penetration occurs when the penetration
! velocity is equal to the rod velocity (UP = VR). At this point the rod begins to behave as a
! rigid body.

        IF(RT.LT.YP.AND.VR.LE.SQRT(2.0*(YP-RT)/RHO_T))EXIT

! If the penetration is greater than the thickness of the target, perforation is achieved terminate
! loop

        IF(P.GT.THK)EXIT

! If the instantaneous length is less than zero, then the rod had totally eroded, Terminate Loop

        IF(LI.LT.0.0)EXIT

! Output data for graphical processing

        WRITE(12, 100), T, VR, UP, P, LI

100      FORMAT(F10.7, 5X, F15.10, 5X, F15.10, 5X, F10.8, 5X, F10.8)

! Time increment, 1 microsecond step size

        T=T+0.000001

    END DO

    PRINT*, EPSI

END PROGRAM Pertubation

```

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